



Client: Donegal County Council

## **Flood Risk Assessment Report**

### **Proposed Housing Development, Carn Road, Gleneely, Co. Donegal**

By: Bernard McLaughlin  
BEng (Hons). MIEI

Date: October 2023

## Report Control



Document: Flood Risk Assessment Report

Project: Proposed Housing Development, Carn Road, Gleneely, Co. Donegal

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Job No: F2941

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## 1.0 INTRODUCTION

Donegal County Council Housing, Corporate & Culture Services team are seeking planning approval for proposed site of 10 residential dwellings. The site identified for the proposed development is located on the southern outskirts of Gleneely village, Co. Donegal.

The development will have 1 phase and units will be constructed running parallel to the site road (R238) frontage, in an aim to meeting the core objectives for housing as outlined in the Donegal County Development Plan 2018-2024 Table 2A.6: The Core Strategy Table.

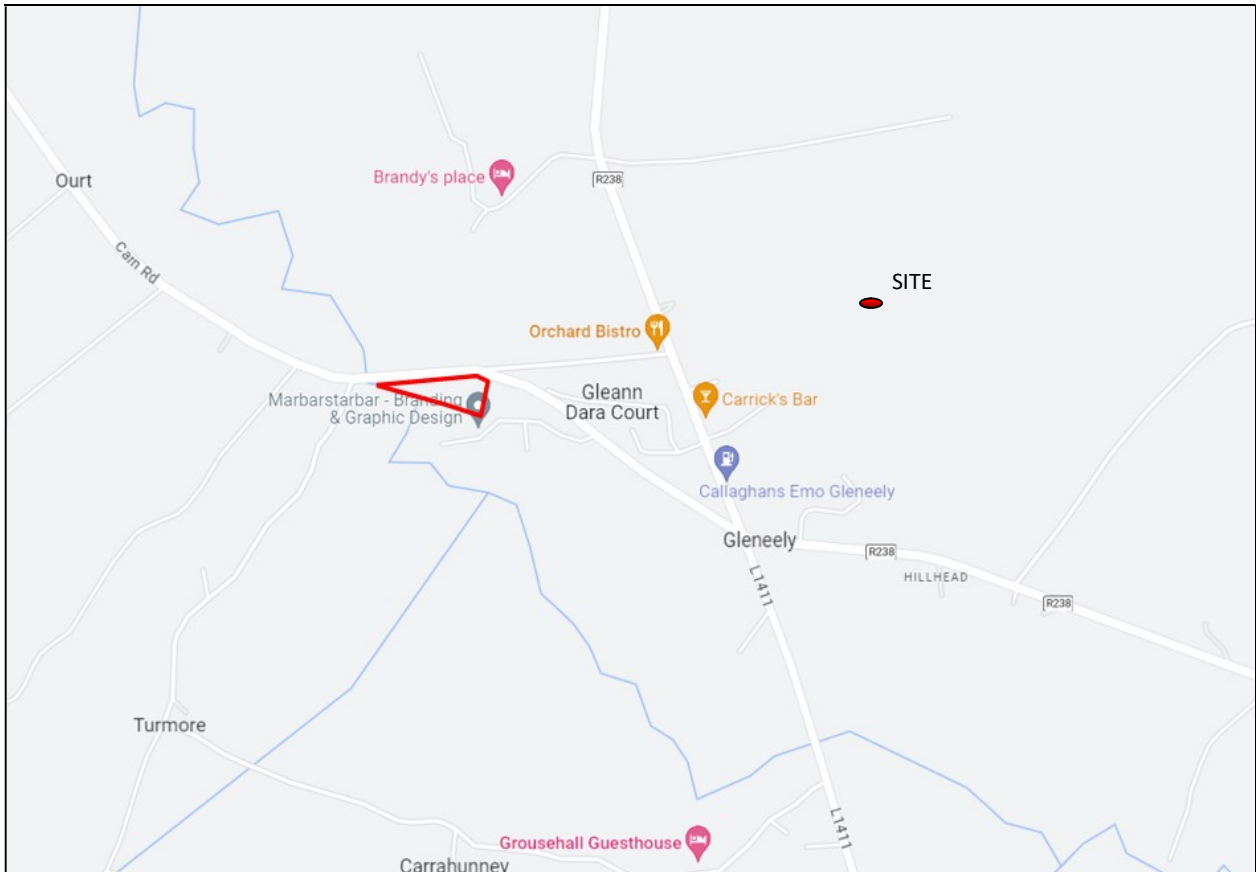
A site-specific flood risk assessment has been requested as part of the planning application process. This flood risk assessment will assess the site in terms of the likelihood of flooding and resultant consequences, while assessing the potential, post development risks in regard to the design of mitigation and compensation measures.

The Flood Risk Assessment (FRA) will be completed in accordance with the Flood Risk Management Guidelines, DEHLG, 2009 (or as updated) including 'Surface Water Drainage Calculations.

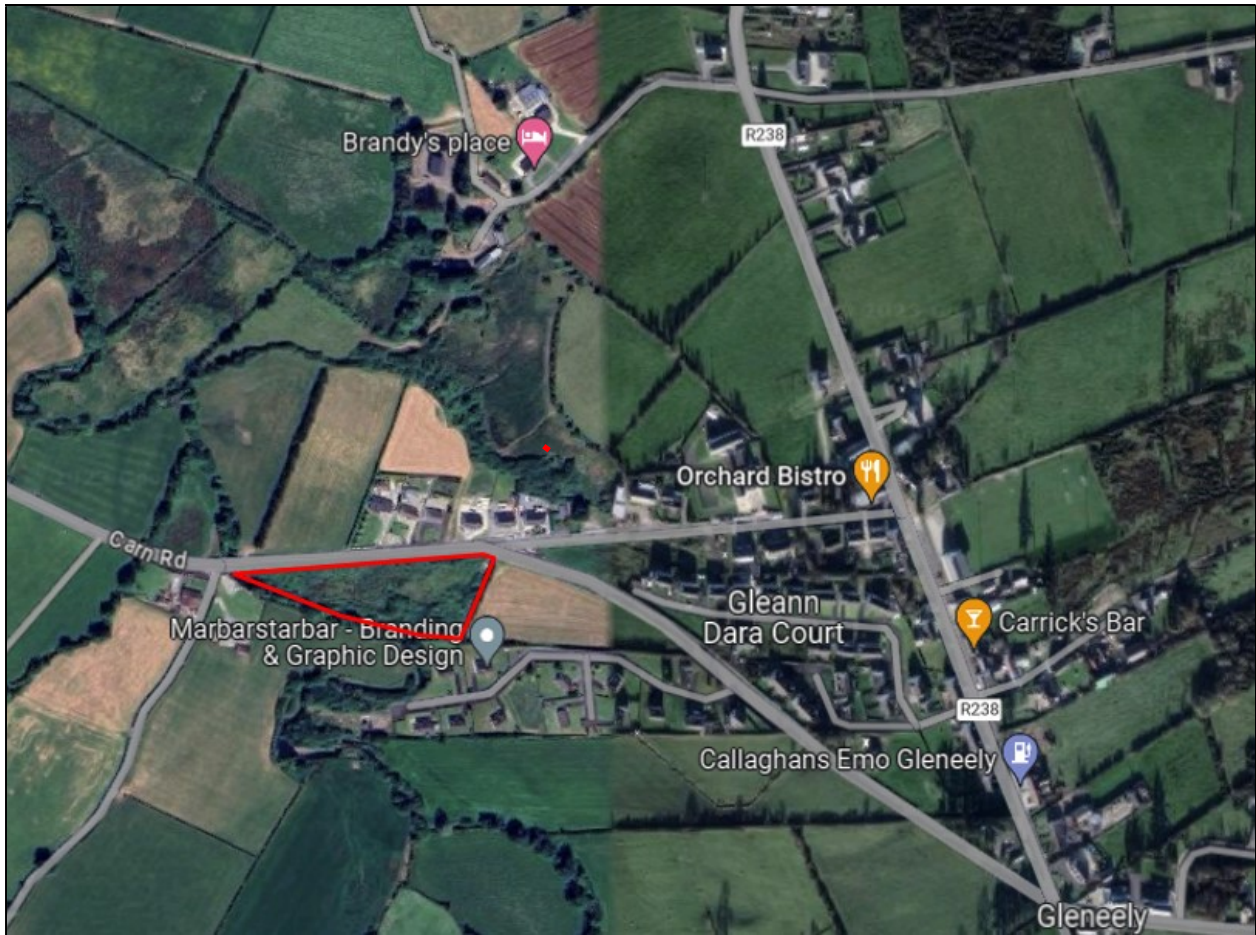
## 2.0 THE SITE

The site identified for the proposed development is located on the southern outskirts of Gleneely village, Co. Donegal. The site has a watercourse known as Gleneely River running parallel to the southern boundary, flowing from East to West converging with Culdaff River before entering the Culdaff Estuary with the North Atlantic Ocean.

The site has an area of approximately 0.88 Hectares and details of the site location and boundaries are provided on Figures 1 and 2.



**Figure 1: Site Location Map (Google Maps)**



**Figure 2: Site Boundary Map**

## 2.1 Site Description

The site is accessed from the Carn Road (R238), through the existing Agriculture Access. The site is bounded to the North by the Carn Road (R238) and to the South by the Gleneely River. The west of the site is a formed point at the existing Bridge for the Gleneely River to flow under the Carn Road (R238). The east of the site is bounded by agricultural land.

The site is currently an undeveloped Greenfield site. with unmaintained overgrown hedge lines, shrubbery, hawthorns and rushes. The site is currently not being utilised for any purpose. Site Photos from a walk over survey can be found in Appendix A.

## 2.2 Watercourse

The site has a watercourse known as Gleneely River running parallel to the southern boundary, flowing from East to West converging with Culdaff River before entering the Culdaff Estuary with the North Atlantic Ocean.

### 3.0 FLOOD IMPACT ASSESSMENT

#### 3.1 Methodology

To facilitate the completion of the FRA, the following methodology was adopted:

- Firstly, background data in relation to the site and its locale, including topographical information, was collated, to gain a general appreciation of the topography of the site and its key features.
- Next a site visit/walk over survey was carried out.
- A desktop study was undertaken with respect to the flooding history of the site. This information is presented in the following sections of this report.
- Detailed design of storm drainage system including attenuation measures required was carried out for the proposed development.
- Flood risk will be evaluated, and conclusions drawn.
- Finally, the production of FRA in accordance with the requirements of the project objectives as defined by Donegal County Council will be completed.

#### 3.2 Site Topographical Information

A topographical survey of the proposed development sites and surrounding lands was provided by Donegal County Council. This survey was to establish the general topography of the site, to enable assessment of potential flood zones and the current drainage layout to be developed. The Key site features include:

- The topographical survey indicates the site is dense with vegetation and briars.
- The site predominantly falls Northeast to Southwest, with the highest level recorded of 38.80m.
- The lowest level recorded is 31.00m and is located along the Top pf the Bank along southern boundary of the proposed site.

A further Topographical Survey was requested to cover Gleneely Riverbed and lands south of the river. This was requested to allow for the assessment of the flood plains and risk to the proposed site. Both Topographical Surveys can be found in Appendix I.

### 3.3 Relevant planning policy

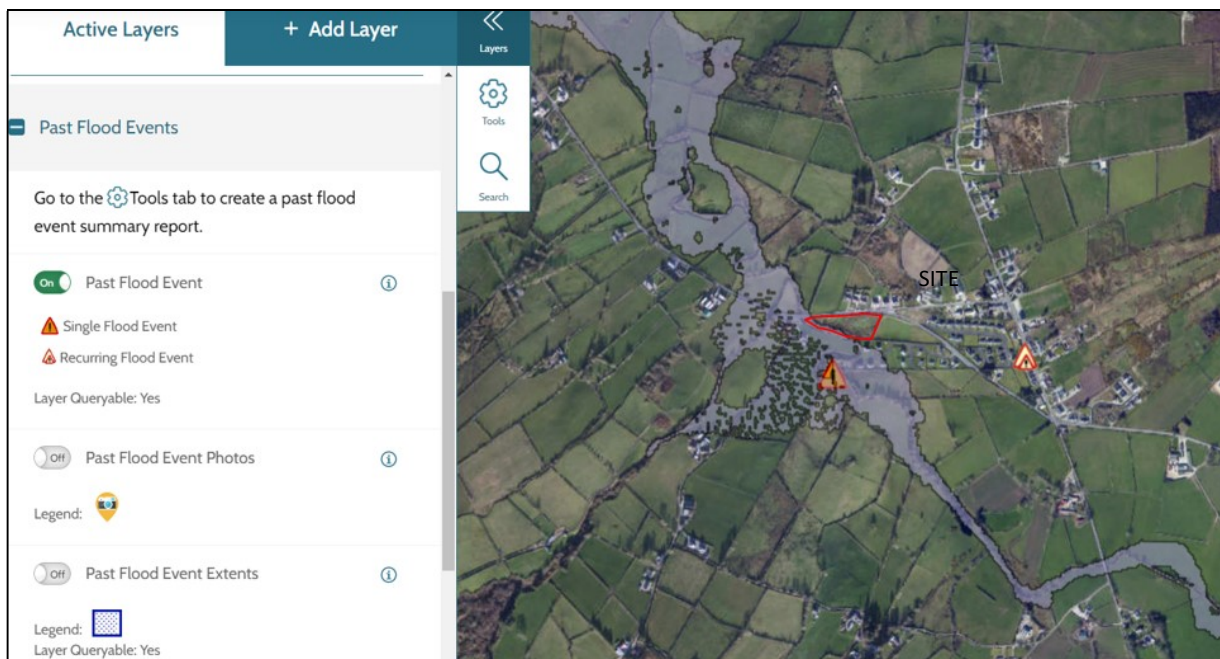
The relevant planning policy with respect to floodplain development is the County Donegal Development Plan 2018-2024, Chapter 5; where the core objectives are:

- F-O-1: To assess all development proposals in accordance with The Planning System and Flood Risk Management Guidelines for Planning Authorities, November 2009, DoEHLG or any amendment to it.
- F-O-2: To adopt a sequential approach to flood risk management when assessing the location for new development based on avoidance, reduction, and mitigation of flood risk.
- F-O-3: To ensure that the requirements of EU and national law in relation to the natural environment and nature conservation are complied with at all stages of flood risk management and to comply with Article 6 of the Habitats Directive and have regard to the relevant conservation objectives, qualifying interests, and threats to the integrity of Natura 2000 sites.

### 3.4 Previous Flooding of the Site

Investigation into the historic flooding of the site does not indicate that the proposed site or the lands immediately neighboring the proposed site are prone to flooding as illustrated on the relevant OPW National Flood Hazard Map reproduced in Figure 3. (Refer to Appendix B for full OPW Flood Hazard Map and report). The flood maps do confirm extensive flooding to the lands further South, upstream of the proposed site south of the Fox Wood Housing development.

Examination of the OSI 25 Inch and 6 Inch maps do not identify areas 'Liable to Flood' on the proposed site or any of the neighboring sites. (Refer to Appendix D)



**Figure 3: OPW Flood Maps- Past Flooding Event**

### 3.5 National CFRAM Programme

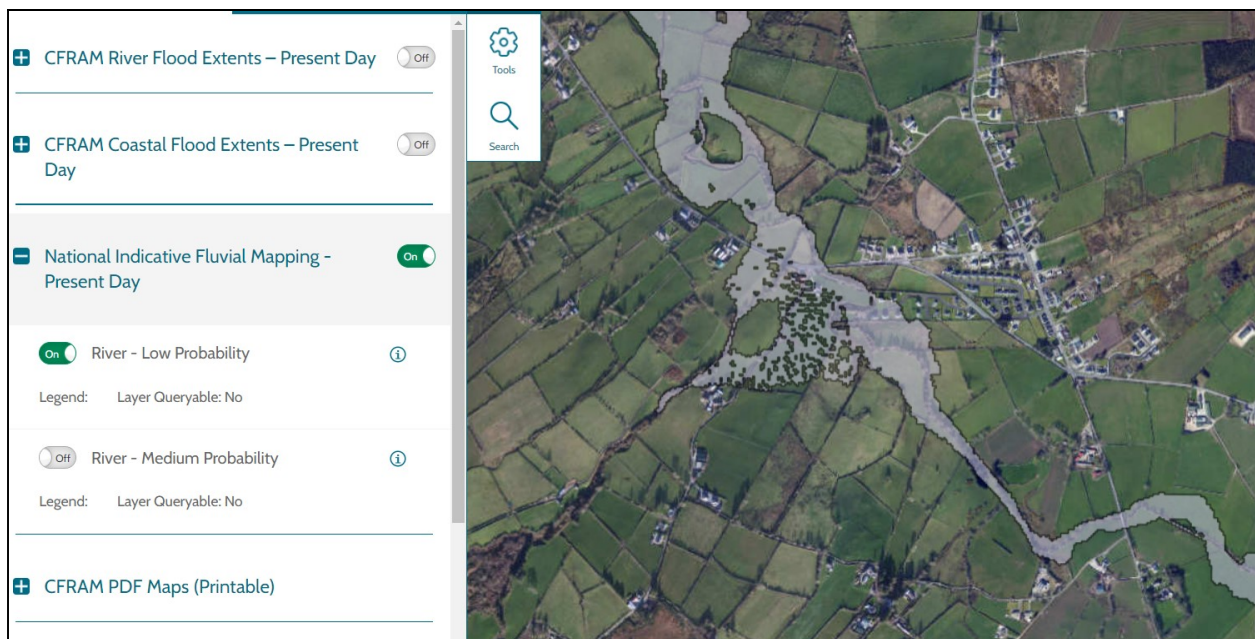
The National CFRAM Programme has three principal milestones:

- Preliminary Flood Risk Assessment (Completed 2011)
- Preparation of Flood Maps (2013-2014)
- Preparation of Flood Risk Management Plans (2015)

Flood zones are geographical areas within which the likelihood of flooding is in a particular range, and they are a key tool in flood risk management within the planning process as well as in flood warning and emergency planning.

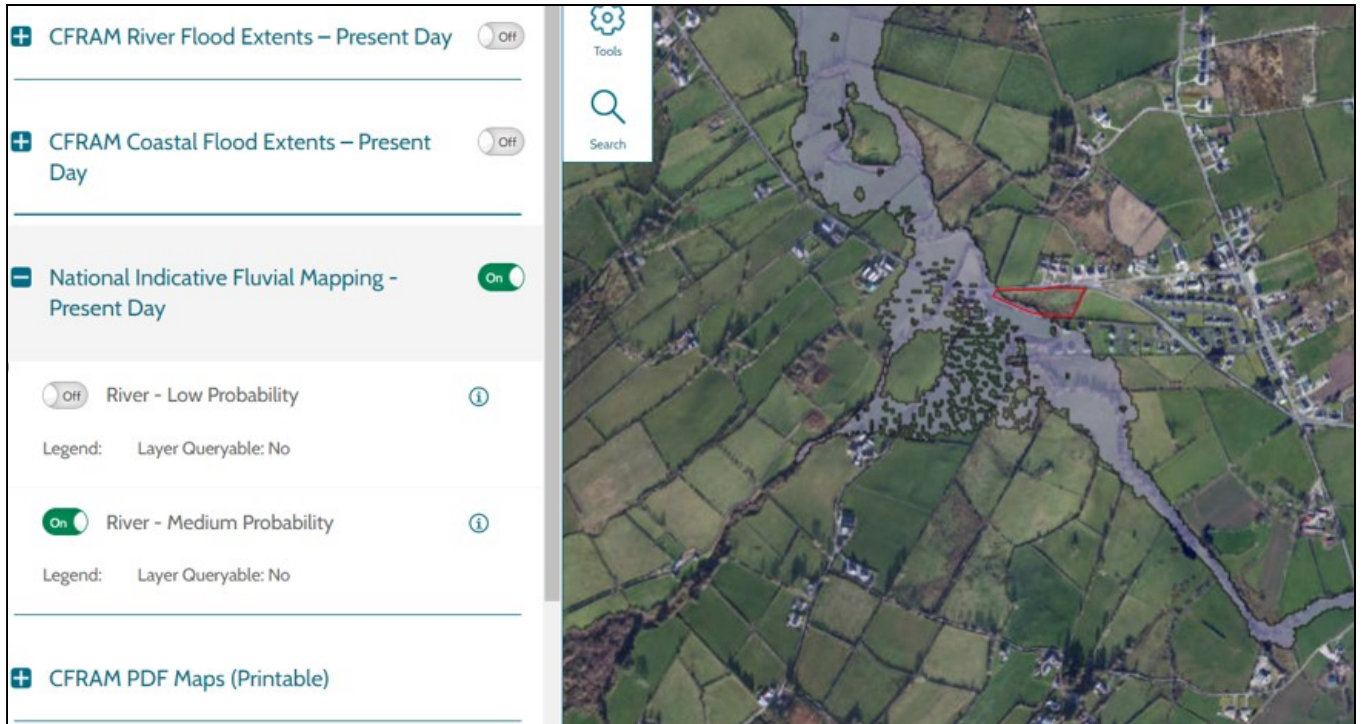
A flood Zone A is defined as high probability of flooding, i.e.) more than 1% probability or 1 in 100 from rivers and more than 0.5% probability or 1 in 200 from coastal flooding. A flood Zone B is defined as moderate probability of flooding, i.e.) between 0.1% probability or 1 in 1,000 years and 1% or 1 in 100 years for river flooding and between 0.1% or 1 in 1,000 years and 0.5% or 1 in 200 for coastal flooding.

The site is not covered by any CFRAM flood maps, however the National Indicative Fluvial Mapping – Present day would indicate that part of the proposed site may fall within both flood Zone A or B. See Figure 4, 5 and 6 below:

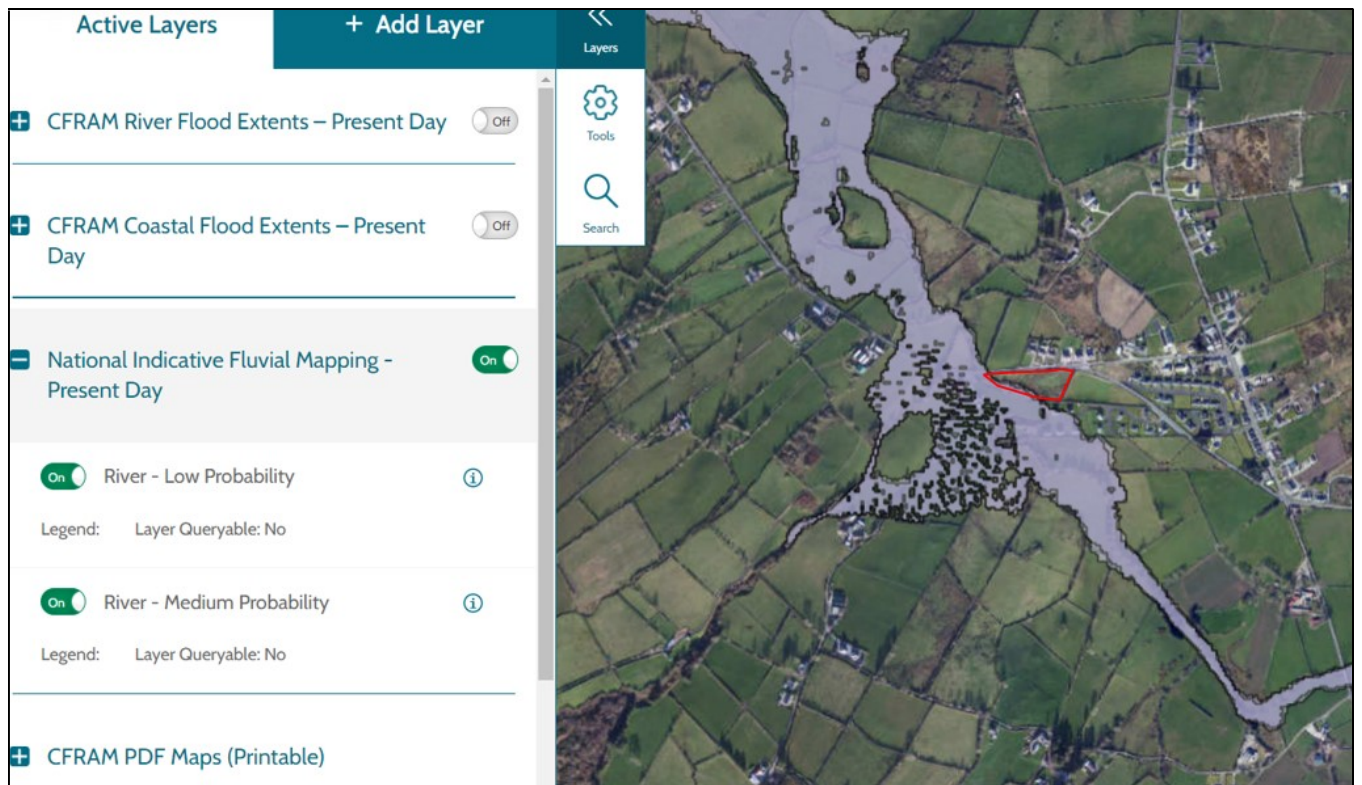


**Figure 4:** National Indicative Fluvial Mapping – Present day (Low Probability)





**Figure 5:** National Indicative Fluvial Mapping – Present day (Medium Probability)



**Figure 6:** National Indicative Fluvial Mapping – Present day (Low + Medium Probability)

### **3.6 Potential Archaeological Site**

Examination of the OSI 25 Inch and 6 Inch maps do not identify anything of Archaeological interest on the proposed site. Refer to Appendix D for OSI maps.

### **3.7 Existing Site Drainage**

The existing site is Greenfield in nature and typically open with isolated whin bushes, brambles and a low-level grass covering. The southern boundary on the site is extensively overgrown with whin bushes and brambles etc. thus making the walkover survey extremely difficult and impossible in places. The open grass areas have substantial coverage of the Common rush, also known as Soft Rush, (*Juncus effusus*), which indicates land drainage is poor or non-existent. The rainfall that currently falls on the site either flows towards the Gleneely River, or lower lying areas and ponds or percolates into the site's sub-soil.

### **3.8 Proposed Development**

The proposed development of the site consists of 10 housing units with associated site works to include an access road, car parking, footpaths, and landscaping. A full copy of the proposed development is contained within Appendix H.

As part of the proposed development, separate storm and foul networks will be constructed. The new storm sewer for the proposed development will discharge into the Gleneely River to the southern boundary of the site. The proposed storm drainage system will incorporate a Hydro-brake and attenuation storage to limit the proposed site to the greenfield run-off rate to ensure there will be no increase in storm water discharge as a result of the proposed development.

The Foul sewer for the proposed development will be designed to connect to an on-site treatment facility to Donegal CC and Irish Water Standards.

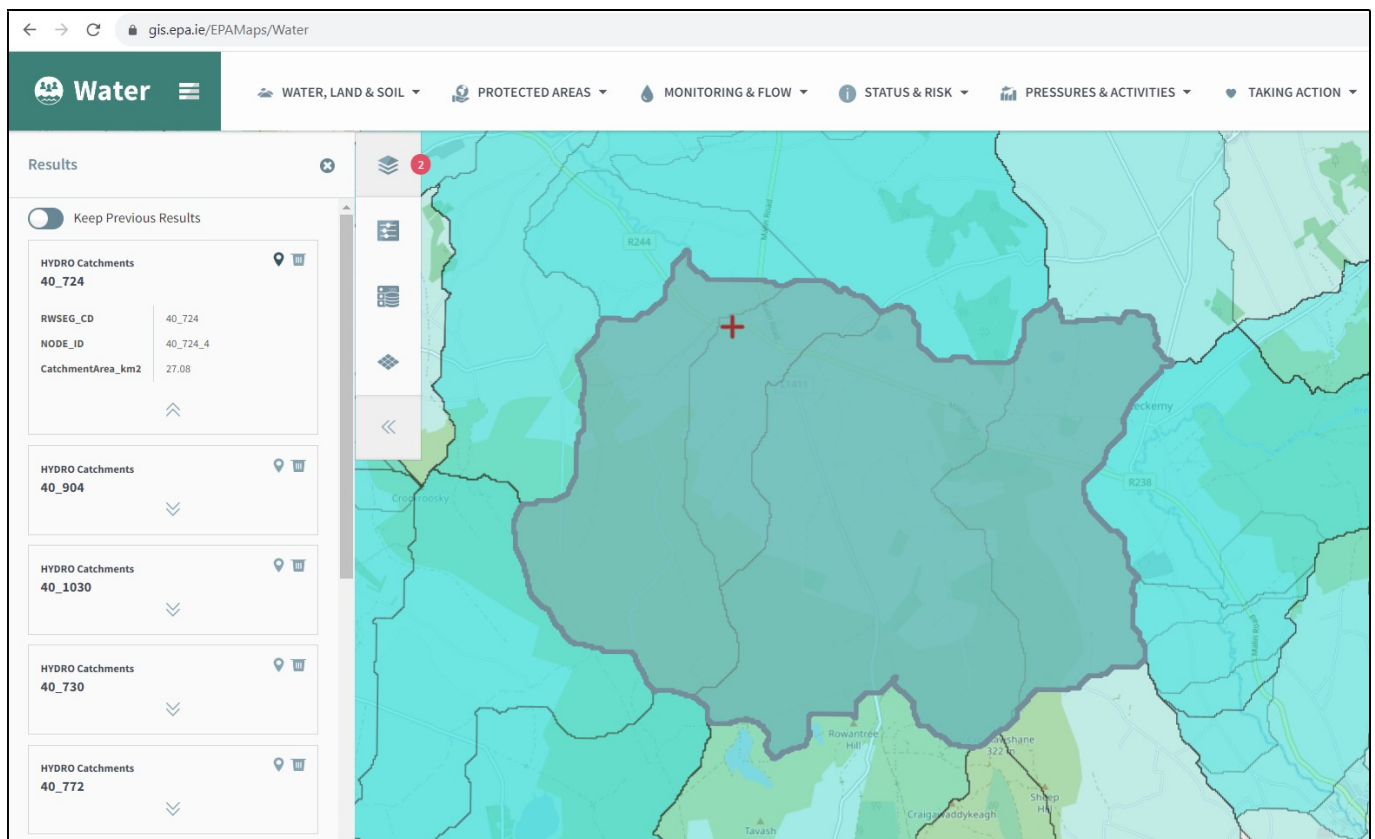
An indicative storm drainage layout for the proposed development is contained within Appendix G of this report.

### 3.9 Flood Impact Evaluation

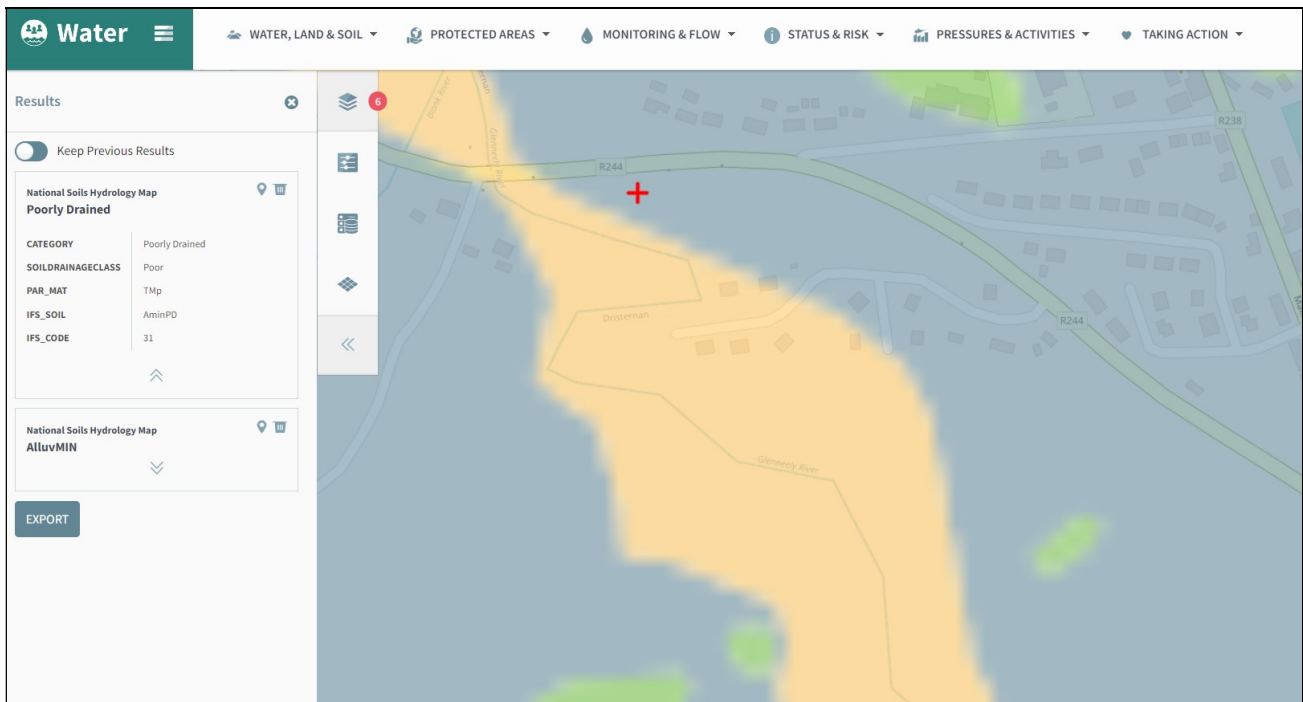
The OPW Flood Maps and reports do not record any flooding or re-occurring flooding at the proposed site. A review of the OPW Flood maps indicate the site is not covered by any generated CFRAM Flood Maps. However, the National Indicative Fluvial Mapping indicates fluvial flooding (1:100yr and 1:1000yr) to the proposed site.

#### 3.9.1 Desktop Study – Q100 Calculation

To provide more clarity on the Q100 flood levels within the site, a desk top study was carried out to determine the extents on the flooding on the site. To calculate the Q100  $Q_{BAR}$  the catchment area for river Gleneely running past the site was generated. This was carried out using Catchments.ie website as shown below in Figure 7. The catchment for the proposed site was calculated as 27.08 km<sup>2</sup>. The soil hydrology classification was also determined from the Catchments.ie website. The soil is deemed to be poorly drained as shown in figure 8 below.



**Figure 7: Catchment Area for Carn Road Site, Gleneely (<https://gis.epa.ie/EPAMaps/Water>)**



**Figure 8: Soil Hydrology for Carn Road Site, Gleneely (<https://gis.epa.ie/EPAMaps/Water>)**

Once the catchment area and Soil Hydrology classification was determined, the information was used as part of the calculation for the Q100 Q<sub>BAR</sub>. The Q100 was calculated using the HR Wallingford method within the uksuds.com Greenfield runoff tool. The runoff estimation approach was the IH124 method. The IH124 equation estimates Q<sub>bar</sub> with the following equation:

$$Q_{\text{bar rural}} = 0.00108 \times (0.01 \times \text{AREA})^{0.89} \times \text{SAAR}^{1.17} \times \text{SPR}^{2.17}, \text{ m}^3/\text{s}$$

Where:

- Q<sub>bar rural</sub> is the mean annual flood flow from a rural catchment (approximately 2.3-year return period).
- AREA is the area of the catchment in ha.
- SAAR is the standard average annual rainfall for the period 1941 to 1970 in mm (SAAR 41-70). SAAR 61-90, which was analysed for FEH for rainfall from 1961 - 1990, is virtually the same and can also be used.
- SPR is Standard Percentage Runoff coefficient for the SOIL category.

The Q100 was calculated using the HR Wallingford method within the uksuds.com Greenfield runoff tool, which generated the existing Q<sub>BAR</sub> l/sec, and predictive 1 in 30 years, 1 in 100 years and 1 in 200 years. Figure 9 shows calculated Q<sub>BAR</sub> l/sec for each scenario where the full calculation sheet can be seen within Appendix C.

**IH124 method**

IH124 specifically addresses the runoff from small catchments (Institute of Hydrology, 1994). Although shown to be slightly less accurate than more recent FEH based methods, it is still considered to be an acceptable approach for assessing greenfield runoff rates.

For more information on the IH124 method, check our [FAQ](#).

**IH124 input fields**

Enter criteria needed to calculate stormwater requirements with the IH124 method.

Derivation of Qbar

The IH124 method estimates Qbar from SPR and SAAR. Alternatively Qbar can be entered manually.

Specify how Qbar should be derived ⓘ

Specify how SPR should be derived ⓘ

Specify SOIL type ⓘ

SPR ⓘ

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**Results using the IH124 method**

Estimated site discharges

|                         | My values                             | Map values                            |
|-------------------------|---------------------------------------|---------------------------------------|
| Qbar (l/s) ⓘ            | <input type="text" value="15525.13"/> | <input type="text" value="5860.52"/>  |
| Greenfield runoff rates |                                       |                                       |
| 1 in 1 year (l/s)       | <input type="text" value="13196.36"/> | <input type="text" value="4981.44"/>  |
| 1 in 30 years (l/s)     | <input type="text" value="25616.47"/> | <input type="text" value="9669.86"/>  |
| 1 in 100 years (l/s)    | <input type="text" value="30274.01"/> | <input type="text" value="11428.01"/> |
| 1 in 200 years (l/s)    | <input type="text" value="33379.04"/> | <input type="text" value="12600.12"/> |

**Figure 9: Greenfield Runoff rate Estimation for Carn Road Site, Gleneely**  
 (<https://www.uksuds.com/tools/members/greenfield-runoff-rate-estimation-members>)

### 3.9.2 Desktop Study – Q100 Flood Zone Determination

Following the determination of the Q100 Greenfield Runoff rate of 30,274.01 l/s, it was converted to m<sup>3</sup>/s to be able to aid in the generation of a flood plain. A Discharge rate of 30.274m<sup>3</sup> for the Q100 allowed for plotting of the Q100 using the Manning Equation. A number of cross sections were surveyed on the site ranging from Cross section A-A to F-F. Information from each cross section was input to the Manning Equation Calculator and through trial and error of increasing the Wetted Perimeter and Area until a Discharge Q value matched or slightly greater than the Q100 Discharge rate of 30.274m<sup>3</sup> was achieved. This allowed for a flood plain to be plotted on each cross section and interpolated onto plan form. The Manning equation calculator used is shown in Figure 10.

| Manning Equation Calculator  | Open channel flow software  |                            |       |                          |     |                         |          |            |       |                    |                  |                                   |                  |
|--|---|----------------------------|-------|--------------------------|-----|-------------------------|----------|------------|-------|--------------------|------------------|-----------------------------------|------------------|
| <p style="text-align: center;"><b>Solve for:</b></p> <p style="text-align: center;">Velocity and Discharge <input type="button" value="v"/></p> <p style="text-align: center;"><b>Select units:</b></p> <p style="text-align: center;">Use meters and seconds units <input type="button" value="v"/></p> <p style="text-align: center;">© 2014 LMNO Engineering.<br/>Research, and Software, Ltd.<br/><a href="http://www.LMNOeng.com">http://www.LMNOeng.com</a></p>  | <p style="text-align: center;"><input type="button" value="Click to Calculate"/></p> <p style="text-align: right;">k = 1.0</p> <table style="width: 100%; border-collapse: collapse;"> <tr><td style="border: 1px solid black;">Area, A (m<sup>2</sup>):</td><td style="border: 1px solid black; text-align: right;">202.5</td></tr> <tr><td style="border: 1px solid black;">Wetted Perimeter, P (m):</td><td style="border: 1px solid black; text-align: right;">9.5</td></tr> <tr><td style="border: 1px solid black;">Channel Slope, S (m/m):</td><td style="border: 1px solid black; text-align: right;">0.000125</td></tr> <tr><td style="border: 1px solid black;">Manning n:</td><td style="border: 1px solid black; text-align: right;">0.014</td></tr> <tr><td style="border: 1px solid black;">Velocity, V (m/s):</td><td style="border: 1px solid black; text-align: right;">Will be computed</td></tr> <tr><td style="border: 1px solid black;">Discharge, Q (m<sup>3</sup>/s):</td><td style="border: 1px solid black; text-align: right;">Will be computed</td></tr> </table> <p style="text-align: center;"><b>Units in Manning calculator:</b> ft=foot, m=meter, s=second.</p> | Area, A (m <sup>2</sup> ): | 202.5 | Wetted Perimeter, P (m): | 9.5 | Channel Slope, S (m/m): | 0.000125 | Manning n: | 0.014 | Velocity, V (m/s): | Will be computed | Discharge, Q (m <sup>3</sup> /s): | Will be computed |
| Area, A (m <sup>2</sup> ):   | 202.5   |                            |       |                          |     |                         |          |            |       |                    |                  |                                   |                  |
| Wetted Perimeter, P (m):   | 9.5   |                            |       |                          |     |                         |          |            |       |                    |                  |                                   |                  |
| Channel Slope, S (m/m):  | 0.000125  |                            |       |                          |     |                         |          |            |       |                    |                  |                                   |                  |
| Manning n:   | 0.014   |                            |       |                          |     |                         |          |            |       |                    |                  |                                   |                  |
| Velocity, V (m/s):   | Will be computed  |                            |       |                          |     |                         |          |            |       |                    |                  |                                   |                  |
| Discharge, Q (m <sup>3</sup> /s):  | Will be computed  |                            |       |                          |     |                         |          |            |       |                    |                  |                                   |                  |
| <p><b>Manning Equation:</b></p> $Q = VA \quad V = \frac{k}{n} \left( \frac{A}{P} \right)^{2/3} S^{1/2}$ <p><small>k is a unit conversion factor: k=1.49 for English units (feet and seconds). k=1.0 for SI units (meters and seconds).<br/> A=Flow area of the pipe, culvert, or channel.<br/> P=Wetted perimeter which is the portion of the circumference that is in contact with water.<br/> Q=Discharge (flow rate).<br/> S=Downward (longitudinal) slope of the culvert.<br/> V=Average velocity in the pipe, culvert, or channel.</small></p> <p><small>Manning n varies with the roughness of the pipe, culvert, or channel. The higher the n, the rougher the material. <a href="#">Table of Manning n values.</a></small></p> <p><small>The Manning Equation is the most commonly used equation to analyze open channel flows. It is a semi-empirical equation for simulating water flows in channels and culverts where the water is open to the atmosphere, i.e. not flowing under pressure, and was first presented in 1889 by Robert Manning. The channel can be any shape - circular, rectangular, triangular, etc. The units in the Manning equation appear to be inconsistent; however, the value k has hidden units in it to make the equation consistent. The Manning Equation was developed for uniform steady state flow (see <a href="#">Discussion and References for Open Channel Flow</a>). S is the slope of the energy grade line and <math>S=h_f/L</math> where <math>h_f</math> is energy (head) loss and L is the length of the channel or reach. For uniform steady flows, the energy grade line = the slope of the water surface = the slope of the bottom of the channel.</small></p> <p><small>The product A/P is also known as the hydraulic radius, <math>R_h</math>.</small></p> |   |                            |       |                          |     |                         |          |            |       |                    |                  |                                   |                  |

**Figure 10: Manning Equation Calculator (<https://www.lmnoeng.com/manning.php>)**

### 3.9.3 Desktop Study – Q100 Findings

Plotting the Q100 it was determined the highest level reached within the floodplain was 33.42m. To further safeguard against the risk of flooding and effects of the climate changes, Foyle Consulting Engineers recommends that a minimum freeboard of 600mm should be provided to the access road, and therefore a finished level of 34.02m. Furthermore, the FFL of the Dwellings should be set at a minimum of 150mm above surrounding Ground Level. The provision of this freeboard is a precaution will ensure the new houses or the access road does not flood during the 1 in 100 yr. fluvial event.

The extent of the Flood Zone will not be affected in any way by the proposed development as there will be no increase in storm water discharge, no loss of flood plain volume and the calculated flood water levels will not be altered as a result of the development. This will result in no net increase in the discharge to the neighbouring water courses and therefore will not increase flood risk to the proposed site or neighboring sites.

### **3.10 Existing Site-Specific Flood Risks**

This section of the report considers site specific flood risk factors which could potentially result in flooding incidents within the development. The site-specific flood risks are likely to result from the following three causes:

#### **3.10.1 Flooding of watercourses**

Blockages obstructing the Gleneely River around the proposed site could constrict flow and cause localised flooding. It is essential that all local water courses are properly maintained by the landowners responsible. As long as the water courses are properly maintained then the National Indicative Fluvial maps clearly show that the site will have minimal risk from fluvial flooding up to and including the 1:1000 yr. rainfall event along its southern boundary.

The proposed development access road will run along the southern boundary and will be a buffer between the residential areas and the watercourse will reduce the probability of the flood risk to homes and careful consideration of Finished Floor Levels for the dwellings will result in a low flood risk from this source.

#### **3.10.2 Overland flow from high ground surrounding the site.**

Lands surrounding the proposed site generally fall from north to south. The proposed development will have longitudinal road gradient between 1:20 and 1:100 with crossfall gradients of 1:40 for footpaths and roads. The overland flow from high ground surrounding the site will not present a risk due the following reasons:

- Lands to the North and West are developed, and all rainwater will be contained within their own individual networks.
- The undeveloped lands to the east of the proposed site have similar levels to the proposed site and the rainfall that currently falls on this undeveloped site currently flows towards the lower lying levels that exist along its southern boundary. Any fall towards our site will be intercepted by an existing sheough on the dividing boundary.

In summary the lands surrounding of the proposed site are predominantly developed with access roads and associated storm sewers which will intercept the overland flow. There are no recorded flooding problems in the surrounding established developments, so the most likely source of flooding would be resulting from a failure of the storm water drainage system. Provided this system is maintained then the risk of flooding to the proposed development from this source is considered to be low.

#### **3.10.3 Surcharged Storm water system**

The third and final risk is pluvial flooding resulting from water escaping from the surcharged storm water network. The development proposes the discharge of water into the Gleneely River. When the local watercourses are in flood then this water has the potential to back up within the storm water drainage system and cause flooding. However, an

appropriately designed storm water drainage system should negate this risk. Careful consideration of the level of the outlet pipe combined with a well-designed storm water drainage system incorporating additional capacity / attenuation provision as appropriate, with ongoing maintenance should result in a low flood risk from this source.

The review of the site-specific flood risks determined a few sources and pathways for flooding to this site and each of these are considered to be low risk at present.



### 3.11 Justification Test

Where there are insufficient sites available to locate development outside flood risk areas, it may be necessary to meet the objectives of proper planning and sustainable development, for development to be sited within flood risk areas.

The Justification Test is an examination of such proposals against proper planning and sustainable development criteria and, if these are satisfied, against flood risk criteria to ensure that risks are reduced to an acceptable level and that flood risk is not increased elsewhere.

Determination if a Justification Test is required, the proposed developed is assessed using the following tables taken from the County Donegal Development Plan 2018-2024 (as varied).

County Donegal Development Plan 2018-2024

**Table 5.4.1: Classification of Vulnerability for different types of development taken from Table 3.1 of The Planning System and Flood Risk Management - Guidelines for Planning Authorities (DoEHLG, 2009)**

| Vulnerability Class  | Land Use and Types of Development which include  |
|--|--|
| <b>Water Compatible Development</b>  | Flood control infrastructure.  |
|  | Docks, marinas and wharves.  |
|  | Navigation facilities.   |
|  | Ship building, repairing and dismantling, dockside fish processing and refrigeration and compatible activities requiring a waterside location.   |
|  | Water based recreation and tourism (excluding sleeping accommodation).   |
|  | Lifeguard and coastguard stations.   |
| <b>Less Vulnerable Development</b>   | Amenity open space, outdoor sports and recreation and essential facilities such as changing rooms, and; Essential ancillary sleeping or residential accommodation for staff required by uses in this category (subject to a specific warning and evacuation plan). |
|  | Buildings used for: retail, leisure, warehousing, commercial, industrial and non-residential institutions.   |
|  | Land and buildings used for holiday or touring non-static holiday caravans and camping, subject to specific warning and excavation plans.  |
|  | Land and buildings used for agriculture and forestry.  |
|  | Waste treatment (except landfill and hazardous waste).   |
| <b>Highly Vulnerable Development</b>   | Mineral working and processing, and;   |
|  | Local transport infrastructure.  |
|  | Garda, ambulance, fire stations and command centres should be operational during flooding.   |
|  | Hospitals.   |
|  | Emergency access and egress points.  |
|  | Schools.   |
|  | Dwelling houses, student halls of residence and hostels.   |
|  | Residential care homes, children's homes and social services homes.  |
| Caravans and mobile home parks.  |  |
| Dwelling houses designed, constructed or adapted for the elderly or, other people with impaired mobility, and;   |  |
| Essential infrastructure, such as primary transport and utilities distribution, including electricity generating power stations and sub-stations, water and sewage treatment, and potential significant sources of pollution in the event of flooding. |  |

Source - Planning System and Flood Risk Management Guidelines for Planning Authorities, November 2009 DoEHLG.

**Table 5.4.2: Matrix of Vulnerability Versus Flood Zone as taken from Table 3.1 of The Planning System and Flood Risk Management - Guidelines for Planning Authorities (DoEHLG, 2009)**

|                                      | <b>Flood Zone A<br/>High Probability</b> | <b>Flood Zone B<br/>Moderate Probability</b> | <b>Flood Zone C<br/>Low Probability</b> |
|--------------------------------------|--|--|---|
| <b>Water Compatible Development</b>  | Development Appropriate                  | Development Appropriate                      | Development Appropriate                 |
| <b>Less Vulnerable Development</b>   | Justification Test Required              | Development Appropriate                      | Development Appropriate                 |
| <b>Highly Vulnerable Development</b> | Justification Test Required              | Justification Test Required                  | Development Appropriate                 |

Consideration of the proposed development with Table 5.4.1 above would confirm the Vulnerability Class as Highly Vulnerable Development (Dwelling Houses). Under further consideration of Table 5.4.2 the proposed development falls within Flood Zone A and B, therefore the development could be deemed subject to a Justification Test.

Review of the proposed site plan has identified only a small portion of the southern boundary is impacted by Flood Zone A and B, with the proposed dwellings all outside these zones. With the proposed layout indicating the access road will be within the Flood Zone A and B, a review of Table 5.4.1 (Local transport infrastructure) and consideration of Table 5.4.2 (Flood Zone A) the development is deemed subject to a Justification Test.

This development is considered integral to meeting the core objectives for housing as outlined in the Donegal County Development Plan 2018-2024 Table 2A.6: The Core Strategy Table.

### 3.12 Application of the Justification Test

The following information box is taken from the County Donegal Development Plan 2018-2024 (as varied).

**Application of the Justification Test in development management**

5.15 Where a planning authority is considering proposals for new development in areas at a high or moderate risk of flooding that include types of development that are vulnerable to flooding and that would generally be inappropriate as set out in Table 3.2, the planning authority must be satisfied that the development satisfies all of the criteria of the Justification Test as it applies to development management outlined in Box 5.1 below.

**Box 5.1 Justification Test for development management (to be submitted by the applicant)**

When considering proposals for development, which may be vulnerable to flooding, and that would generally be inappropriate as set out in Table 3.2, the following criteria must be satisfied:

1. The subject lands have been zoned or otherwise designated for the particular use or form of development in an operative development plan, which has been adopted or varied taking account of these Guidelines.
2. The proposal has been subject to an appropriate flood risk assessment that demonstrates:
  - (i) The development proposed will not increase flood risk elsewhere and, if practicable, will reduce overall flood risk;
  - (ii) The development proposal includes measures to minimise flood risk to people, property, the economy and the environment as far as reasonably possible;
  - (iii) The development proposed includes measures to ensure that residual risks to the area and/or development can be managed to an acceptable level as regards the adequacy of existing flood protection measures or the design, implementation and funding of any future flood risk management measures and provisions for emergency services access; and
  - (iv) The development proposed addresses the above in a manner that is also compatible with the achievement of wider planning objectives in relation to development of good urban design and vibrant and active streetscapes.

The acceptability or otherwise of levels of residual risk should be made with consideration of the type and foreseen use of the development and the local development context.

Note: See section 5.27 in relation to major development on zoned lands where sequential approach has not been applied in the operative development plan.

Refer to section 5.28 in relation to minor and infill developments.

#### 3.12.1 Step 1 – Zoned Lands

In the first step for the proposed site Justification Test, while considering proposals for development, which may be vulnerable to flooding, and that would generally be inappropriate as set out in Table 3.2, the subject lands would be required to have been zoned or otherwise designated for the particular use or form of development in an operative development plan, which has been adopted or varied taking account of these Guidelines.

In accordance with the County Donegal Development Plan 2018-2024 the site is identified as outside of the Settlement Boundary as seen in Map 15.41 Gleneely within Appendix E.

However, the site is bounded to the south with the Gleneely River, it is still in proximity to numerous residential dwellings on the Carn road, and Fox Wood housing development.

### 3.12.2 Step 2 – Appropriate Flood Risk Assessment

Step 2 under the Justification test is to determine the proposal has been subject to an appropriate flood risk assessment that demonstrates the criteria in Box 5.1. For this assessment each point has been taken separately and detailed below:

***i. The development proposed will not increase flood risk elsewhere and, if practicable, will reduce overall flood risk.***

The proposed development has only partial affected areas covered by Flood Zone A and B. The developed site will collect the rainfall within dedicated Storm sewer network with a discharge manhole supply the existing Gleneely River. The Storm Sewer discharge will be limited to Green Field run off and controlled by a flow control device.

The 0.88 ha application site is currently an undeveloped Greenfield site, with unmaintained overgrown hedge lines, shrubbery, hawthorns, and rushes. The site is currently not being utilised for any purpose. The majority of the site is considered to have a permeable surface area. The rainfall on the current site either flows towards the lower lying areas located to the southern boundary of the site, evaporates or percolates into the subsoil. The Greenfield run-off rate for the existing site has been calculated as 8.80 L/Sec. Attenuation of the rainfall events will be incorporated with the Storm Network using oversized Pipes and Manhole Rings. Limited Storm discharge to Greenfield runoff creates a theoretical Net balance to existing conditions versus future conditions with the impermeable area increased.

***ii. The development proposal includes measures to minimise flood risk to people, property, the economy, and the environment as far as reasonably possible.***

The proposed development has only partial affected areas covered by flood Zone A and B, and no dwellings will be constructed within this area. As described in part “i” the site will be limited to Green field runoff and attenuation of the rainfall events will be incorporated with the Storm Network using oversized Pipes and Manhole Rings. Limited Storm discharge to Greenfield runoff creates a theoretical Net balance to existing conditions versus future conditions with the impermeable area increased. Therefore, the watercourse will not be negatively impacted in the future scenario.

The OPW Flood Maps and reports do not record any flooding or re-occurring flooding at the proposed site. The site is currently not affected by flooding from a 1:200-year Coastal flooding event.

To further safeguard against the risk of flooding and effects of the climate changes, Foyle Consulting Engineers recommends that a minimum freeboard of 600mm should be provided to the access road, and therefore a finished level of 34.02m. Furthermore, the FFL of the Dwellings should be set at a minimum of 150mm above surrounding Ground Level. The provision of this freeboard is a precaution will ensure the new houses or the access road does not flood during the 1 in 100 yr. fluvial event.

The extent of the Flood Zone will not be affected in any way by the proposed development as there will be no increase in storm water discharge, no loss of flood plain volume and the calculated flood water levels will not be altered as a result of the development. This will result in no net increase in the discharge to the neighboring water courses and therefore will not increase flood risk to the proposed site or neighboring sites.

**iii. The development proposed includes measures to ensure that residual risks to the area and/or development can be managed to an acceptable level as regards the adequacy of existing flood protection measures or the design, implementation and funding of any future flood risk management measures and provisions for emergency services access; and**

As described in part "i" the site will be limited to Green field runoff and attenuation of the rainfall events will be incorporated with the Storm Network using oversized Pipes and Manhole Rings. Limited Storm discharge to Greenfield runoff creates a theoretical Net balance to existing conditions versus future conditions with the impermeable area increased. Therefore, the watercourse no not be worse of in the future scenario. The provision of this attenuation is a precaution will ensure the new site does not flood during the 1 in 100 yr. fluvial event.

As previously mentioned, no dwellings will be constructed in Zone A or B flood zones and the road will be constructed at a level of 34.02m and above which includes a freeboard safety factor.

**iv. The development proposed addresses the above in a manner that is also compatible with the achievement of wider planning objectives in relation to development of good urban design and vibrant and active streetscapes.**

Parts I, ii, iii cover details of the proposed storm attenuation and restricted discharge of Greenfield Runoff. They address the wider planning objective, due to the net zero balance to the stream and surrounding areas. The requirement for these houses is highlighted within the County Donegal Development Plan 2018-2024 where this development is considered integral to meeting the core objectives for housing as outlined in the Donegal County Development Plan 2018-2024 Table 2A.6: The Core Strategy Table.

On review of the information the justification weighs in favour of the site to proceed. The site being restricted to Greenfield runoff and incorporating its own attenuation system through large pipes and manhole rings to contain a 1 in 100-year storm event (including Climate Change) therefore resulting in no net increase in the discharge to the neighboring water courses.

The proposed dwellings are situated out of the flood zones and finished floor levels are to be set 150mm above the surrounding ground levels and road network, which will be designed to have a free board above the existing Q100 level.

## **4.0 DEVELOPMENT FEASIBILITY**

### **4.1 Pre-development**

Donegal County Council Housing, Corporate & Culture Services team are seeking planning approval for proposed site of 10 residential dwellings. The development will have 1 phase and units will be constructed running parallel to the site road (R238) frontage, in an aim to meeting the core objectives for housing as outlined in the Donegal County Development Plan 2018-2024 Table 2A.6: The Core Strategy Table.

The site is currently an undeveloped Greenfield site. with unmaintained overgrown hedge lines, shrubbery, hawthorns and rushes. The site is currently not being utilised for any purpose. Site Photos from a walk over survey can be found in Appendix A.

The proposed development has only partial affected areas covered by flood Zone A and B.

### **4.2 Post-development**

The proposed development will consist of 10 new residential dwellings, access road, car parking, landscaping, and associated site works. A plan of the proposed development is contained within Appendix H.

Post development, the site will have an impermeable area of 0.27ha. The developed site will collect the rainfall within dedicated Storm sewer network with a discharge manhole restricting flow to Greenfield run-off with the use of a flow control device. The storm will discharge into the Gleneely River via a Headwall set-up. The Greenfield run-off rate for the existing site has been calculated as 8.80 L/Sec. Attenuation of the rainfall events will be incorporated with the Storm Network using oversized Pipes and Manhole Rings. Limited Storm discharge to Greenfield runoff creates a theoretical Net balance to existing conditions versus future conditions with the impermeable area increased.

Foyle Consulting Engineers used Causeway Flow modelling software to design the Storm system utilising a flow control device with a restricted discharge of 8.80 l/s. Simulations for the 2-year, 30 year and 100-year return period events have been assessed, using Causeway Flow, with a 10% increase in rainfall as a result of climate change included with an additional 10% added to the impermeable drainage area to allow for urban creep. The indicative storm drainage layout for the site is contained within Appendix G of this report. The proposed development internal storm sewer design and construction will be completed to an adoptable standard.

The calculations in Appendix F confirm the proposed site storm drainage system, including the flow control and attenuation, is adequate to provide sufficient storage for the 1 in 100-year storm event plus the 10% climate change allowance. Attenuation is provided in the form of oversized pipes and large diameter manholes creating a storage volume in excess of 59.2m<sup>3</sup> within the road network.

Exceedance conditions result in above ground flood flow occurring either when the capacity of the drainage system is exceeded or where the rate of runoff exceeds the inlet capacity of the drain. Without good design, flood flow will follow default pathways leading to flooding of properties. It is possible to avoid this by setting proposed ground levels that will direct flood flows away from the proposed properties.

The analysis also demonstrates that, whilst the storm drainage system may become surcharged within 300mm of proposed manhole or road gully cover levels during the 1 in 100-year return period event, no out of system flooding will occur. To safeguard against potential pluvial flood risk to the development, final development levels and gradients will be re-profiled as necessary to remove any isolated low-lying areas and/or have appropriate surface water drainage infrastructure installed to remove any standing water. In addition, the finished floor levels of the proposed residential units should be located at least 150mm above adjacent ground levels. In the event that the proposed system becomes surcharged during a storm greater than the 1 in 100yr storm event then the storm water surface flow will be managed to ensure there is no risk of flooding to the proposed properties.

#### **4.3 Post-development-Potential Archaeological Site**

Examination of the OSI 25 Inch and 6 Inch maps do not identify anything of Archaeological interest on the proposed site, however, if during the construction process anything of Archaeological interest is discovered then the appropriate organisations should be informed.

#### **4.4 Overland flow originating from the site and potentially affecting elsewhere.**

The proposed development will increase the storm water runoff rate which has been used for the drainage design for the proposed development to ensure there is no increased risk of flooding on site or off site. There will be no increased risk due the following reasons:

- Proposed development levels selected to direct overland flow towards drainage networks.
- Finished Floor levels will be selected to be 150mm above surrounding ground levels.
- No formal drainage to back gardens, with drainage taking place via percolation through the soil to mimic the natural undeveloped drainage regime.
- The proposed development access roads and sewer network will be designed to intercept any overland flow and direct towards storm drainage system.
- The proposed development storm network system will be designed to include a flow control and attenuation for the 100-year return event.
- Any low-lying area will be re-profiled as part of the proposed development and the overland flow will be intercepted by the network of roads and associated storm drainage system. This will prevent surface water ponding within the proposed development site.

#### **4.5 Foul Drainage**

A foul sewer network will be constructed to an adoptable standard and will transfer foul flows from the constructed residential units to an on-site treatment facility to Donegal CC and Irish Water Standards. Permission to discharge treated effluent into the Gleneely River will be obtained from Donegal County Council prior to the discharge of any foul flows from the proposed site.



## 5.0 Conclusion

Foyle Consulting Engineers have prepared this Flood Risk Assessment to be submitted in support of the Full Planning Application for the proposed development.

In summary:

- The proposed development site consists of 10 residential dwelling housing units with associated site works to include an access road, car parking, footpaths, and landscaping. Separate foul and storm drainage networks will service the development.
- The site is currently an undeveloped Greenfield site. with unmaintained overgrown hedge lines, shrubbery, hawthorns, and rushes. The site is currently not being utilised for any purpose.
- The site identified for the proposed development is located on the southern outskirts of Gleneely village, Co. Donegal. The site has a watercourse known as Gleneely River running parallel to the southern boundary, flowing from East to West converging with Culdaff River before entering the Culdaff Estuary with the North Atlantic Ocean.
- The site has an area of approximately 0.88 Hectares.
- A review of the OPW Flood maps indicate the site is not covered by any generated CFRAM Flood Maps. However, the National Indicative Fluvial Mapping indicates fluvial flooding (1:100yr and 1:1000yr) to the proposed site.
- It is proposed to limit the storm water discharge from the proposed developed site to that of the Greenfield Run-off. Foyle Consulting Engineers calculated a Greenfield run-off rate of 8.80/sec. Causeway Flow Design Report within Appendix F of this report prove that 1 in 100-year storm event will be contained within the proposed storm drainage system that includes a flow control and attenuation storage of 59.2m<sup>3</sup> and therefore is considered to be designed to exceedance.
- The post development storm water discharge rate will be limited by flow control and attenuation to the consented rate. The proposed attenuation measures will be sized up to and including the 100-year rainfall event (plus 10% climate change) and therefore no part of the site floods during a 1 in 100-year return period event. This proposal will be submitted to Donegal County Council for approval. An indicative storm sewer layout for the proposed development is contained within Appendix G of this report.
- To safeguard against potential pluvial flood risk to the development or neighbouring sites, final development levels and gradients will be re-profiled as necessary to remove any isolated low-lying areas and/or have appropriate surface water drainage infrastructure installed to remove any standing water. In addition, the finished floor levels of the proposed residential units should be located at least 150mm above adjacent ground levels. In the event that the proposed system becomes surcharged during a storm greater than the 1 in 100yr storm event then the storm water surface flow will be managed to ensure there is no risk of flooding to the proposed properties.
- The foul sewer network will be designed to transfer foul flows from the constructed residential units to an on-site treatment plant. Also, the foul network system will have to take into consideration the proposed storm water network system as there may be clearance issues at crossover points. Permission to discharge treated effluent into the Gleneely River will be obtained from Donegal County Council prior to the discharge of any foul flows from the proposed site.

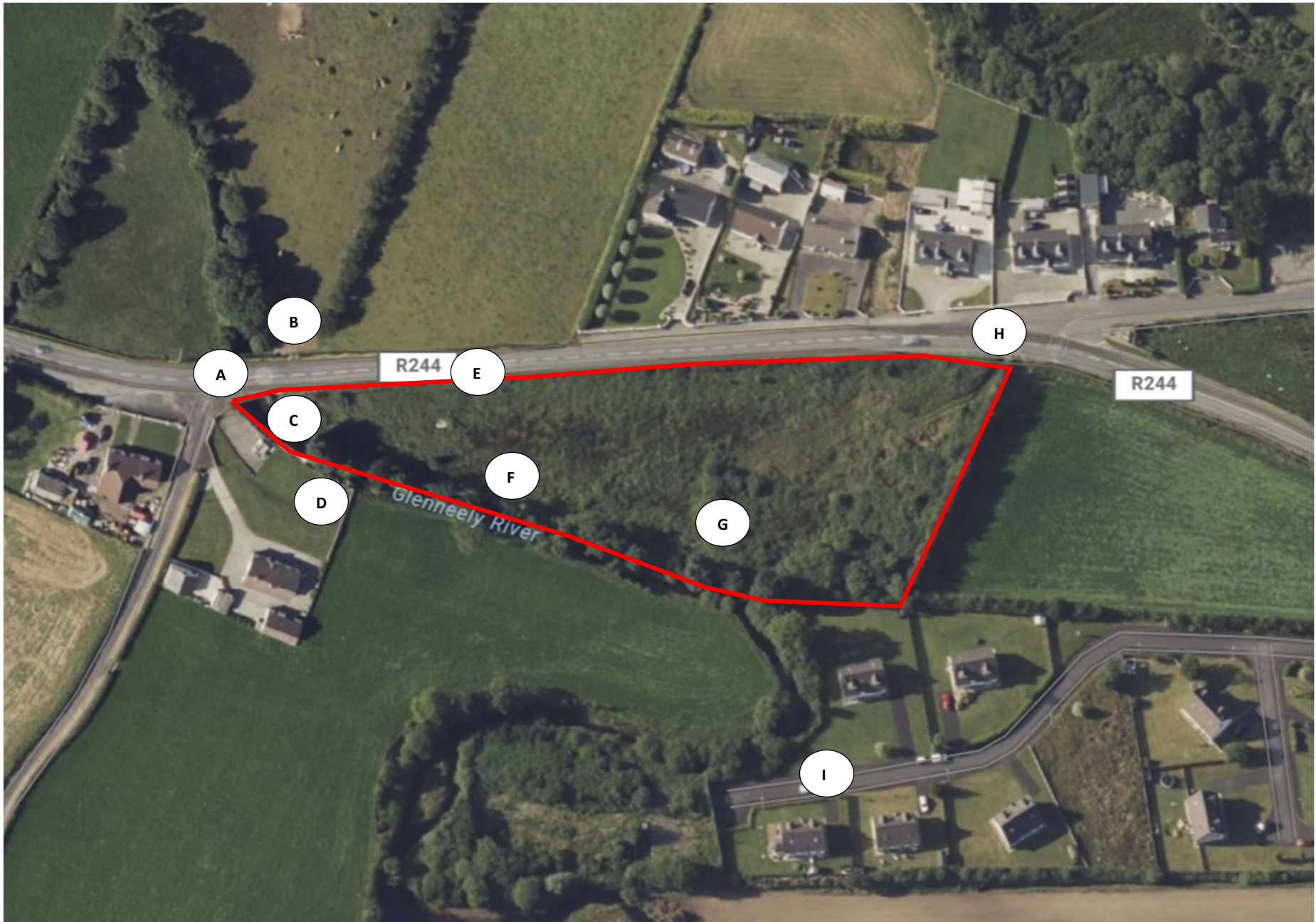
- The preliminary design has therefore shown that an exceedance surface water event can be dealt with without the need to revise the layout of the proposed development.
- Both the foul and storm sewer networks for the proposed development will be designed and constructed to an adoptable standard for Donegal County Council.
- The review of the site-specific flood risks: flooding of watercourses, overland flow from high ground surrounding the site and surcharged storm water systems determined few sources and pathways for flooding to this site and each of these are considered to be low risk at present.
- The proposed development will increase the storm water runoff rate. This increased storm water runoff rate has been used for the drainage design for the proposed development to ensure there is no increased risk of flooding on site or off site.
- This development is considered integral to meeting the core objectives for housing as outlined in the Donegal County Development Plan 2018-2024 Table 2A.6: The Core Strategy Table.

As it has been documented within this report there will be no increased flood risk to the proposed development and no adverse impacts to other developments or features of importance to nature conservation, archaeology, or the built heritage and therefore the proposed developed for this site should be considered acceptable.

# **Appendix A**

## **SITE WALK OVER PHOTOGRAPHS**

Site Walkover Photo Locations

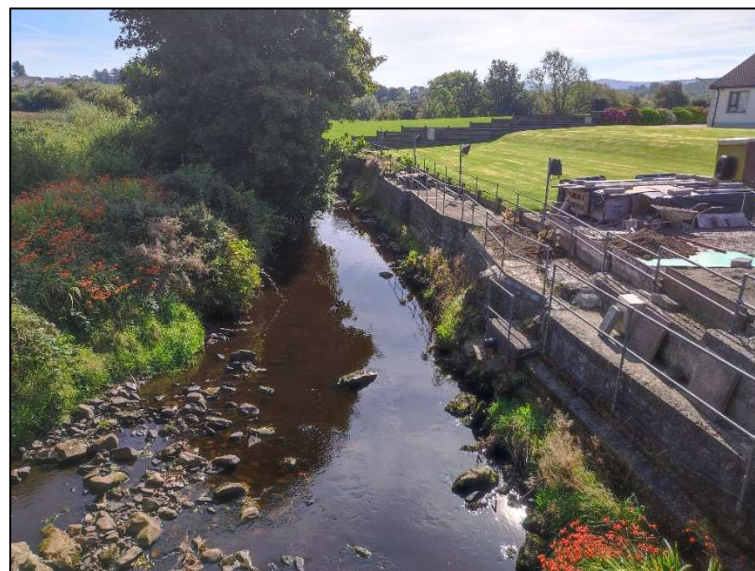


**Site Walkover Photos – Location A**

**(Looking North)**



**(Looking South)**



Site Walkover Photos – Location B

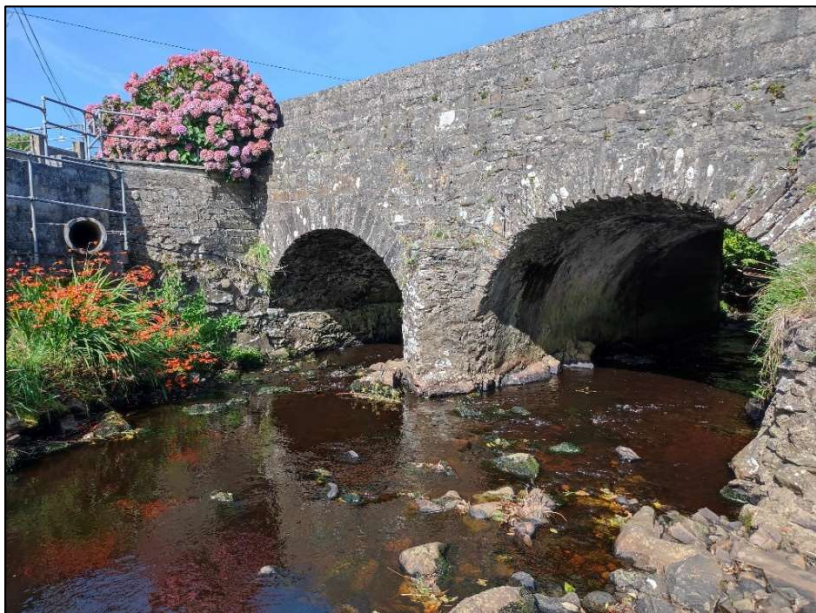




Site Walkover Photos – Location C







Site Walkover Photos – Location D





Site Walkover Photos – Location E





Site Walkover Photos – Location F



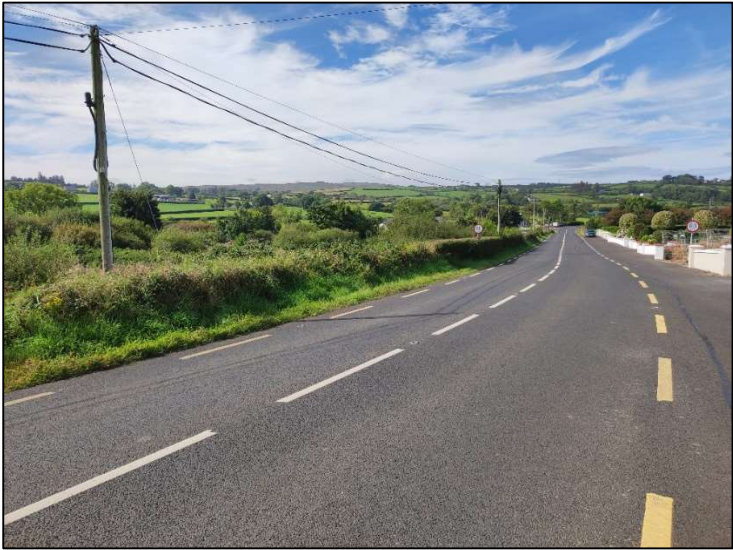
Site Walkover Photos – Location G







Site Walkover Photos – Location H





Site Walkover Photos – Location I



# **Appendix B**

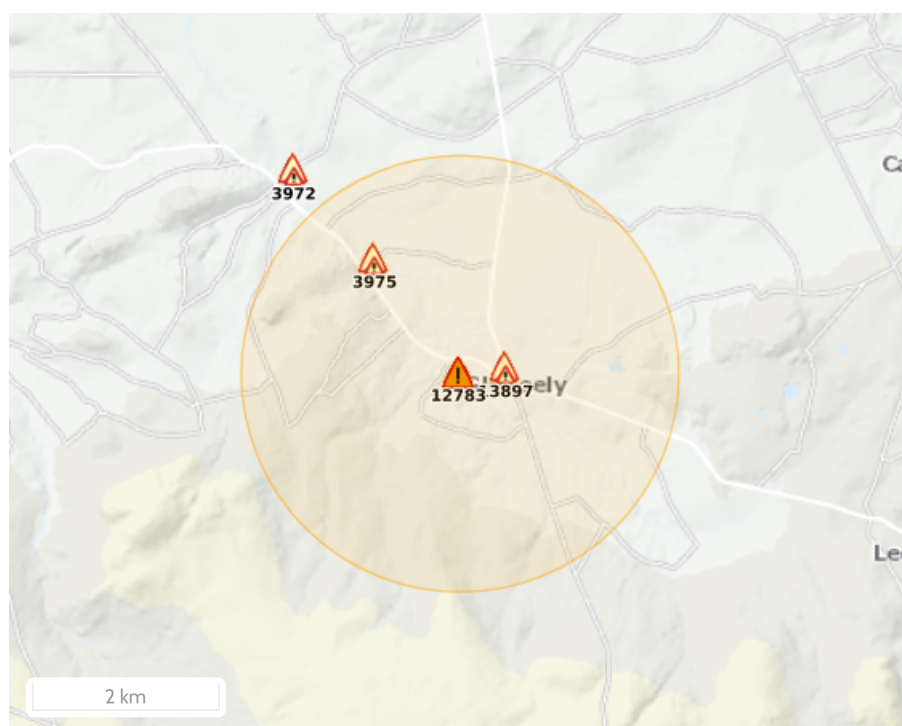
## **OPW FLOODING INFORMATION**



Report Produced: 11/10/2023 12:10

This Past Flood Event Summary Report summarises all past flood events within 2.5 kilometres of the map centre.

This report has been downloaded from [www.floodinfo.ie](http://www.floodinfo.ie) (the "Website"). The users should take account of the restrictions and limitations relating to the content and use of the Website that are explained in the Terms and Conditions. It is a condition of use of the Website that you agree to be bound by the disclaimer and other terms and conditions set out on the Website and to the privacy policy on the Website.



## Map Legend

- Single Flood Event
- Recurring Flood Event
- Past Flood Event Extents
- Drainage Districts Benefited Lands\*
- Land Commission Benefited Lands\*
- Arterial Drainage Schemes Benefited Lands\*

\* Important: These maps do not indicate flood hazard or flood extent. Their purpose and scope is explained on [Floodinfo.ie](http://Floodinfo.ie)

## 3 Results

|    | Name (Flood_ID)   | Start Date | Event Location    |
|----|---|------------|-------------------|
| 1. | Flooding at Gleneely - 2015 (ID-12783)<br>Additional Information: <a href="#">Reports (0)</a> <a href="#">Press Archive (0)</a>       | n/a        | Approximate Point |
| 2. | Flooding at Gleneely - Recurring (ID-13897)<br>Additional Information: <a href="#">Reports (0)</a> <a href="#">Press Archive (0)</a>  | n/a        | Approximate Point |
| 3. | Culdaff River Aghatubrid Recurring (ID-3975)<br>Additional Information: <a href="#">Reports (1)</a> <a href="#">Press Archive (0)</a> | n/a        | Approximate Point |

**MINUTES OF  
MEETING**

**Reference:** P4D403A – F310 – 011 – 004 – 2761 Page 1 of 5

**Project No.:** P4D403A

**Project Title:** OPW Flood Hazard Mapping – Phase 1

**Purpose of Meeting:** Donegal County Council – Oral Report – Area Executive Engineer – Inishowen

**Participating:** Area Roads Manager Donegal County Council  
Area Executive Engineer Donegal County Council  
Supervisors Donegal County Council  
Search Manager ESBI

**Venue:** Carndonagh

**Date of Meeting:** 11/01/06

**Copies to:** Donegal CC  
**Compiled by:** Search Manager ESBI

**Status:** Final

**Approved for ESBI:** Search Manager ESBI

**Approved for Donegal County Council:** Area Executive Engineer

**Date:** 21/03/2006

## Meeting with Electoral Area Engineers for Inishowen 11/01/06

The Electoral Area Engineers and supervisors outlined 57 areas that are or were prone to flooding. These are: -

- C1. Ballygorman/Killure – River overflows its banks every year through a combination of heavy rain and high tides. A significant area is covered.  
Flood Id = 3949
- C2. Stewbridge Bridge 1 – River Glennagannon overflows its banks once or twice a year through a combination of heavy rain and high tides.  
Flood Id = 3950
- C3. Carndonagh - River Glennagannon overflows its banks once or twice a year through a combination of heavy rain and high tides.  
Flood Id = 3952
- C4. Esky Bay – Low lying land is flood by exceptional high tides every year. The road is liable to flood.  
Flood Id = 3955
- C5. Goorey - Low lying land is flood by exceptional high tides every year. A stretch of the R242 is liable to flood.  
Flood Id = 3961
- C6. Malin - Low lying land is flood by exceptional high tides every year. The road is liable to flood.  
Flood Id = 3962
- C7. Carndonagh 2 River Glennagannon overflows its banks every year after heavy rain. The road is liable to flood.  
Flood Id = 3966
- C8. Culdaff- River Culdaff overflows its banks every year after heavy rain. A significant area is covered.  
Flood Id = 3968
- C9. Gleneely - River Culdaff overflows its banks every year after heavy rain. A significant area is covered.  
Flood Id = 3972
- C10. Aghatubrid - River Culdaff overflows its banks every year after heavy rain. The road is liable to flood.  
Flood Id = 3975
- C11. Cashel - River Glentogher overflows its banks every year after heavy rain.  
Flood Id = 3978
- C12. Glentogher - River Glentogher overflows its banks every year after heavy rain. The road is liable to flood.  
Flood Id = 3979
- C13. Binnion - River Clonmany overflows its banks every year through a combination of heavy rain and high tides. A significant area is covered.  
Flood Id = 3981
- C14. Muff – Liberty and Kilderry streams overflows their banks once or twice a year through a combination of heavy rain and high tides. Road is liable to flood and properties are affected.  
Flood Id = 3985
- C15. Corvish - River Glennagannon overflows its banks once or twice a year through a combination of heavy rain and high tides.  
Flood Id = 3986

- C16. Lackboy - River overflows its banks every year through a combination of heavy rain and high tides.  
Flood Id = 3987
- C17. Cloghorna - River overflows its banks every year through a combination of heavy rain and high tides. One side of the road is liable to flood.  
Flood Id = 3988
- C18. Meenadiff/Glasmullan – A combination of the River Clonmany overflowing its banks and runoff from high land causes flooding every year after heavy rain. The road is liable to flood.  
Flood Id = 3989
- C19. Carrick - River Owenboy overflows its banks every year after heavy rain. A significant area is covered. Properties may be affected.  
Flood Id = 3990
- C20. Magherabane – Runoff from high ground causes flooding every year after heavy rain. The road is liable to flood.  
Flood Id = 3991
- C21. Strogill Beach - River overflows its banks through a combination of heavy rain and high tides. Not every year  
Flood Id = 3992
- C22. Luddan – A combination of low lying flat land and streams overflowing their banks cause flooding every year after heavy rain.  
Flood Id = 3993
- C23. Craigtown - A combination of a river overflowing its banks and runoff from high land causes flooding every year after heavy rain.  
Flood Id = 3994
- C24. Glebe Large - River overflows its banks through a combination of very heavy rain and high tides. The road is liable to flood and properties are affected. Not every year.  
Flood Id = 3995
- C25. Burnfoot 1(The Slab) - River Burnfoot overflows its banks every year through a combination of heavy rain and high tides. A significant area is covered. The road is liable to flood  
Flood Id = 3996
- C26. Burnfoot 2(The Slab) - River Burnfoot overflows its banks every year through a combination of heavy rain and high tides. A significant area is covered. The road is liable to flood and properties are affected  
Flood Id = 3997
- C27. Cristaghkeel - Runoff from high ground causes flooding every year after heavy rain. The road is liable to flood.  
Flood Id = 3998
- C28. Magherabeg - River overflows its after very heavy rain. Not every year.  
Flood Id = 3999
- C29. Ballymagae - Runoff from high ground causes water to flow down the road into a property after very heavy rain  
Flood Id = 4000
- C30. Ross Point - River overflows its banks every year through a combination of heavy rain and high tides. The land is low lying and is protected by embankments. Development is taking place in the area.  
Flood Id = 4001



- C31. Mill Bay - Low lying land is flood by exceptional high tides approximately once every year. The road is liable to flood.  
Flood Id = 4002
- C32. Baylet – Fresh water lake level rises every year and floods a significant area after heavy rain.  
Flood Id = 4003
- C33. Ballyederowen 1 - River Burnfoot overflows its banks every year after heavy rain.  
Flood Id = 4004
- C34. Ballyederowen 2 - Runoff from high ground causes flooding after very heavy rain approximately once every 5 years. The road is liable to flood.  
Flood Id = 4005
- C35. Lagnadavaugh - Runoff from high ground causes flooding after very heavy rain approximately once every 5 years. The road is liable to flood.  
Flood Id = 4006
- C36. Garvary - Runoff from high ground causes flooding after very heavy rain approximately once every 2 years. The road is liable to flood.  
Flood Id = 4007
- C37. Glen Bridge - River Burnfoot overflows its banks every year after heavy rain. The road is liable to flood.  
Flood Id = 4008
- C38. Ballyederowen 3 – A combination of low lying land and Rivers Burnfoot and Skeoge overflowing their banks every year due to heavy rain and high tides.  
Flood Id = 4009
- C39. Skeoge Road - River Skeoge overflows its banks once or twice a year through a combination of heavy rain and high tides. Road is liable to flood approximately once every 5 years  
Flood Id = 4010
- C40. Bridge End 1 - River Skeoge overflows its banks every year after heavy rain. The road is liable to flood.  
Flood Id = 4011
- C41. Bridge End 2 - Runoff from high ground causes flooding after very heavy rain approximately once every 2 years. The road is liable to flood.  
Flood Id = 4012
- C42. Bridge End 3 - Runoff from high ground causes flooding after very heavy rain approximately once every 2 years. The road is liable to flood.  
Flood Id = 4013
- C43. Inch – Low lying land floods every year after heavy rain. A significant area is flooded  
Flood Id = 4014
- C44. Trady Point – Low lying land floods every year after heavy rain. A significant area is flooded  
Flood Id = 4015
- C45. Carrownmaddy - Runoff from high ground causes flooding after very heavy rain approximately once every 2 to 3 years. The road is liable to flood.  
Flood Id = 4016
- C46. Bridge End 4 - Runoff from high ground causes flooding after very heavy rain approximately once every 2 years. The road is liable to flood.  
Flood Id = 4017

- C47. Blanket Nook - Low lying land floods every year after heavy rain. A significant area is flooded  
Flood Id = 4018
- C48. Glar - Low lying land floods every year after heavy rain. A significant area is flooded  
Flood Id = 4019
- C49. Moyle - River overflows its banks every year after heavy rain.  
Flood Id = 4020
- C50. Moylemoss - River overflows its banks every year after heavy rain.  
Flood Id = 4021
- C51. Newtown Cunningham 1 - A combination of low lying land and a stream overflowing its banks every year due to heavy rain and high tides. County Council pump house is affected.  
Flood Id = 4022
- C52. Newtown Cunningham 2 - A combination of a river overflowing its banks and runoff from high land causes flooding every year after heavy rain. The road is liable to flood and properties are affected.  
Flood Id = 4023
- C53. Murlough - A combination of low lying land and a stream overflowing its banks every year due to heavy rain and high tides.  
Flood Id = 4024
- C54. Roosky - A combination of low lying land flat land and runoff from high land cause flooding every year after heavy rain. The road is liable to flood. The problem has been exacerbated by recent development  
Flood Id = 4025
- C55. Coxtown - Low lying land floods every year after heavy rain.  
Flood Id = 4026
- C56. Carrigans – Stream and River Foyle overflows their banks every year after heavy rain and high tides.  
Flood Id = 4027
- C57. Monglass - Low lying land floods every year after heavy rain.  
Flood Id = 4028

## **Summary**

The council does install, unblock and replace culverts to alleviate flooding

# Appendix C

## Q100 Calculations

|                |                     |
|----------------|---------------------|
| Calculated by: | Bernard McLaughlin  |
| Site name:     | Carn Road, Gleneely |
| Site location: | Gleneely            |

## Site Details

|            |                   |
|------------|-------------------|
| Latitude:  | 55.24107° N       |
| Longitude: | 7.15632° W        |
| Reference: | 54139248          |
| Date:      | Oct 25 2023 15:53 |

This is an estimation of the greenfield runoff rates that are used to meet normal best practice criteria in line with Environment Agency guidance "Rainfall runoff management for developments", SC030219 (2013), the SuDS Manual C753 (Ciria, 2015) and the non-statutory standards for SuDS (Defra, 2015). This information on greenfield runoff rates may be the basis for setting consents for the drainage of surface water runoff from sites.

Runoff estimation approach

## Site characteristics

Total site area (ha):

## Methodology

|                              |                             |
|------------------------------|-----------------------------|
| $Q_{BAR}$ estimation method: | Calculate from SPR and SAAR |
| SPR estimation method:       | Calculate from SOIL type    |

## Notes

(1) Is  $Q_{BAR} < 2.0$  l/s/ha?

When  $Q_{BAR}$  is  $< 2.0$  l/s/ha then limiting discharge rates are set at 2.0 l/s/ha.

## Soil characteristics

|              | Default | Edited |
|--------------|---------|--------|
| SOIL type:   | 2       | 4      |
| HOST class:  | N/A     | N/A    |
| SPR/SPRHOST: | 0.3     | 0.47   |

(2) Are flow rates  $< 5.0$  l/s?

Where flow rates are less than 5.0 l/s consent for discharge is usually set at 5.0 l/s if blockage from vegetation and other materials is possible. Lower consent flow rates may be set where the blockage risk is addressed by using appropriate drainage elements.

## Hydrological characteristics

|                                | Default | Edited |
|--------------------------------|---------|--------|
| SAAR (mm):                     | 1180    | 1180   |
| Hydrological region:           | 13      | 13     |
| Growth curve factor 1 year:    | 0.85    | 0.85   |
| Growth curve factor 30 years:  | 1.65    | 1.65   |
| Growth curve factor 100 years: | 1.95    | 1.95   |
| Growth curve factor 200 years: | 2.15    | 2.15   |

(3) Is  $SPR/SPRHOST \leq 0.3$ ?

Where groundwater levels are low enough the use of soakaways to avoid discharge offsite would normally be preferred for disposal of surface water runoff.

## Greenfield runoff rates

|                       | Default  | Edited   |
|-----------------------|----------|----------|
| $Q_{BAR}$ (l/s):      | 5860.52  | 15525.13 |
| 1 in 1 year (l/s):    | 4981.44  | 13196.36 |
| 1 in 30 years (l/s):  | 9669.86  | 25616.47 |
| 1 in 100 year (l/s):  | 11428.01 | 30274.01 |
| 1 in 200 years (l/s): | 12600.12 | 33379.04 |

This report was produced using the greenfield runoff tool developed by HR Wallingford and available at [www.uksuds.com](http://www.uksuds.com). The use of this tool is subject to the UK SuDS terms and conditions and licence agreement, which can both be found at [www.uksuds.com/terms-and-conditions.htm](http://www.uksuds.com/terms-and-conditions.htm). The outputs from this tool are estimates of greenfield runoff rates. The use of these results is the responsibility of the users of this tool. No liability will be accepted by HR Wallingford, the Environment Agency, CEH, Hydrosolutions or any other organisation for the use of this data in the design or operational characteristics of any drainage scheme.



| REV | DESCRIPTION | BY | CHK | APP | DATE |
|-----|-------------|----|-----|-----|------|
|     |             |    |     |     |      |

Donegal County Council

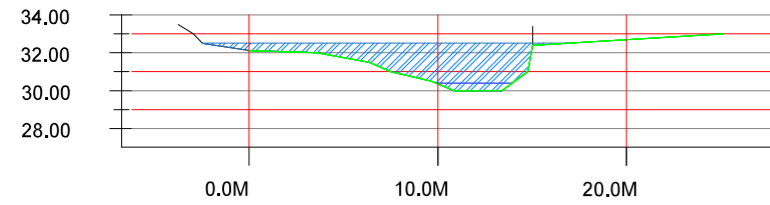
**FOYLE CONSULTING ENGINEERS**  
 HARBOUR OFFICE, PORT ROAD  
 USAHALLY  
 L'DERRY, BT47 6FL

TEL: +44 (0)28 71865757  
 FAX: +44 (0)28 71861656  
 e-mail: admin@foylece.com

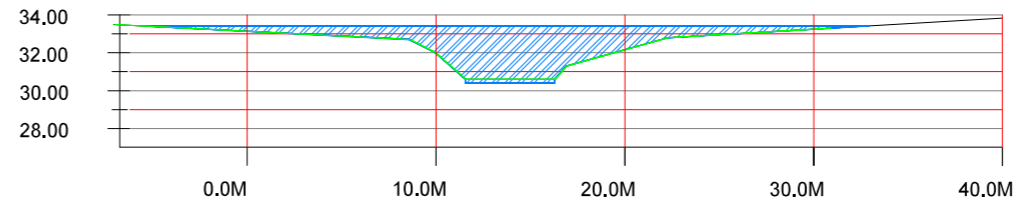
Project:  
Carn Road, Gleneely, Co. Donegal

Drawing Title:  
Proposed Drainage Layout

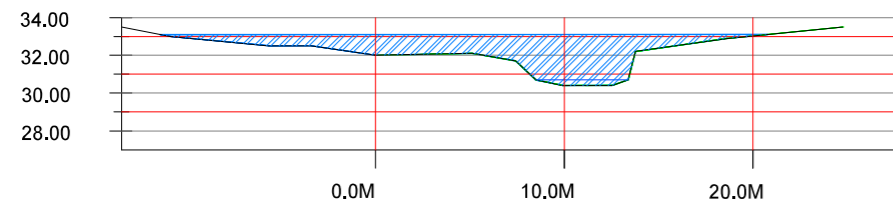
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| A1          | BMcl        | Oct 23   | BMcl    | Oct 23 |
| Project No. | Drawing No. | Revision |         |        |
| F2941       | 005         |          |         |        |



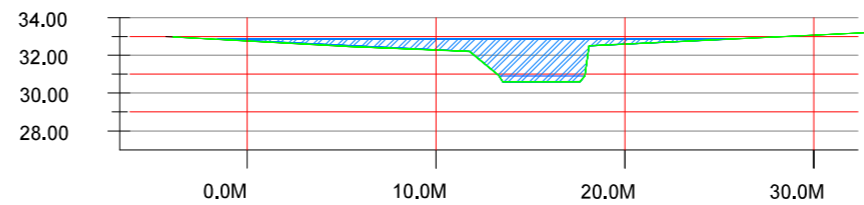
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Vertical Scale 1:500



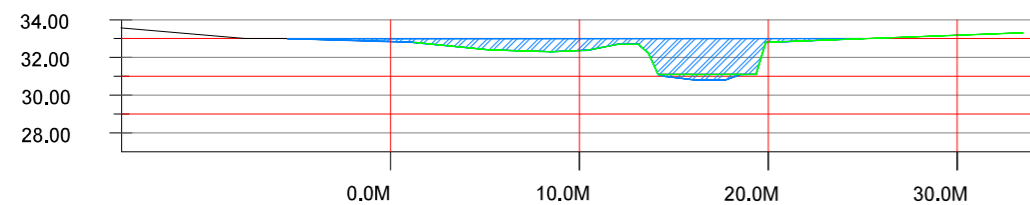
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Vertical Scale 1:500



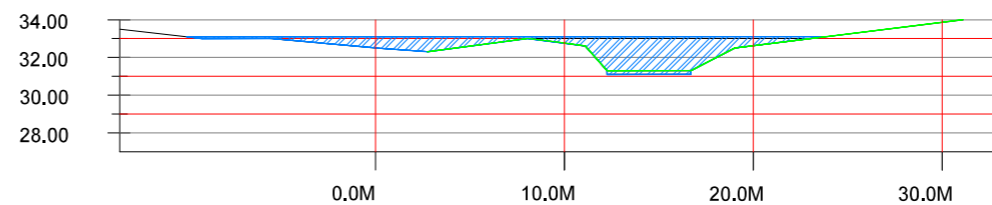
Section C-C  
Horizontal Scale 1:500  
Vertical Scale 1:500



Section D-D  
Horizontal Scale 1:500  
Vertical Scale 1:500



Section E-E  
Horizontal Scale 1:500  
Vertical Scale 1:500



Section F-F  
Horizontal Scale 1:500  
Vertical Scale 1:500

| REV | DESCRIPTION | BY | CHK | APP | DATE |
|-----|-------------|----|-----|-----|------|
|     |             |    |     |     |      |

Donegal County Council

**FOYLE CONSULTING ENGINEERS**  
HARBOUR OFFICE, PORT ROAD  
LISAHALLY  
L'DERRY, BT47 6FL

TEL: +44 (0)28 71865757  
FAX: +44 (0)28 71861656  
e-mail: admin@foylece.com

Project:  
Carn Road, Gleneely, Co. Donegal

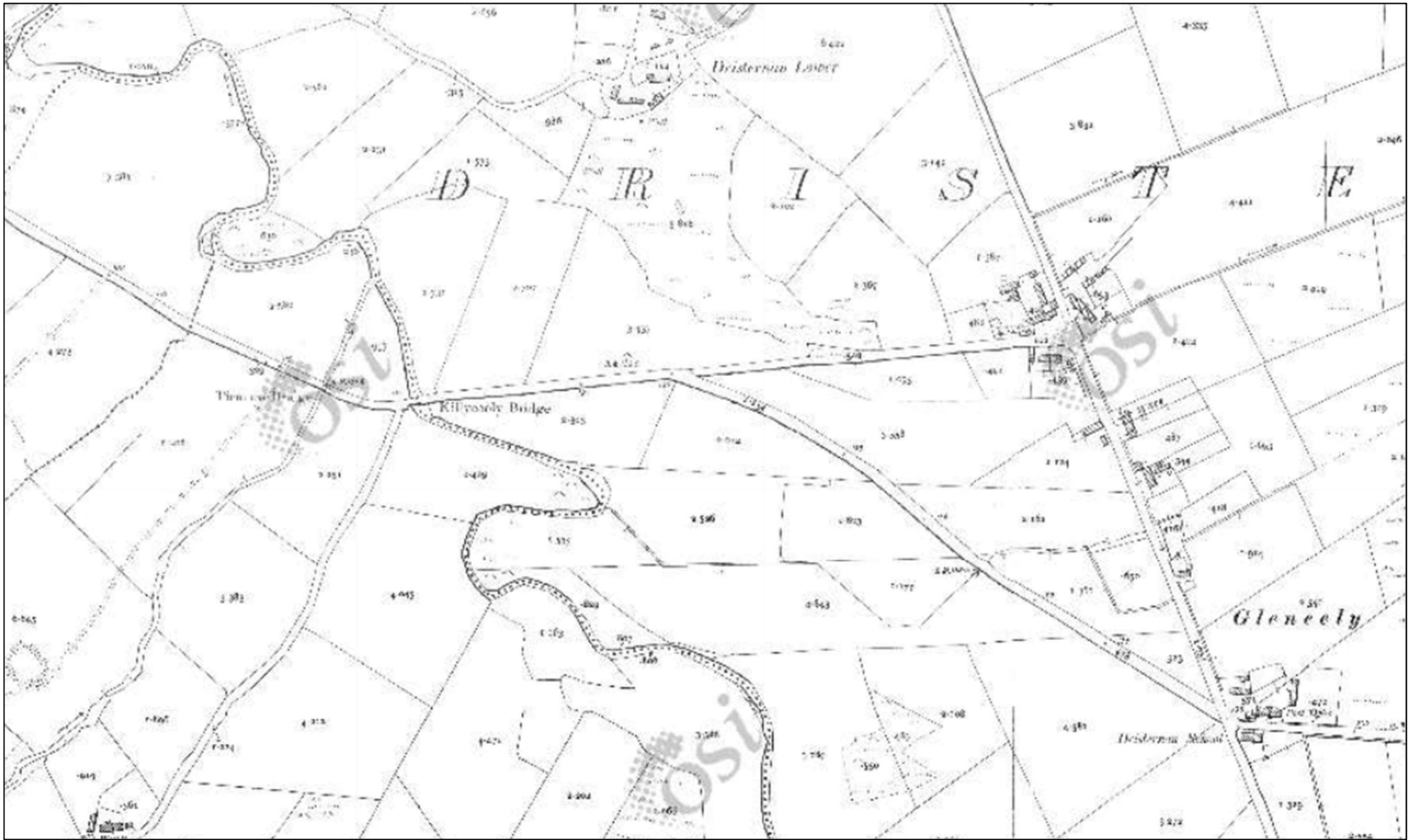
Drawing Title:  
Q100 Cross Sections

| Scale @     | A1    | Drawn       | Date   | Checked  | Date   |
|-------------|-------|-------------|--------|----------|--------|
| 1:200       |       | BMcl        | Oct 23 | BMcl     | Oct 23 |
| Project No. | F2941 | Drawing No. | 004    | Revision |        |

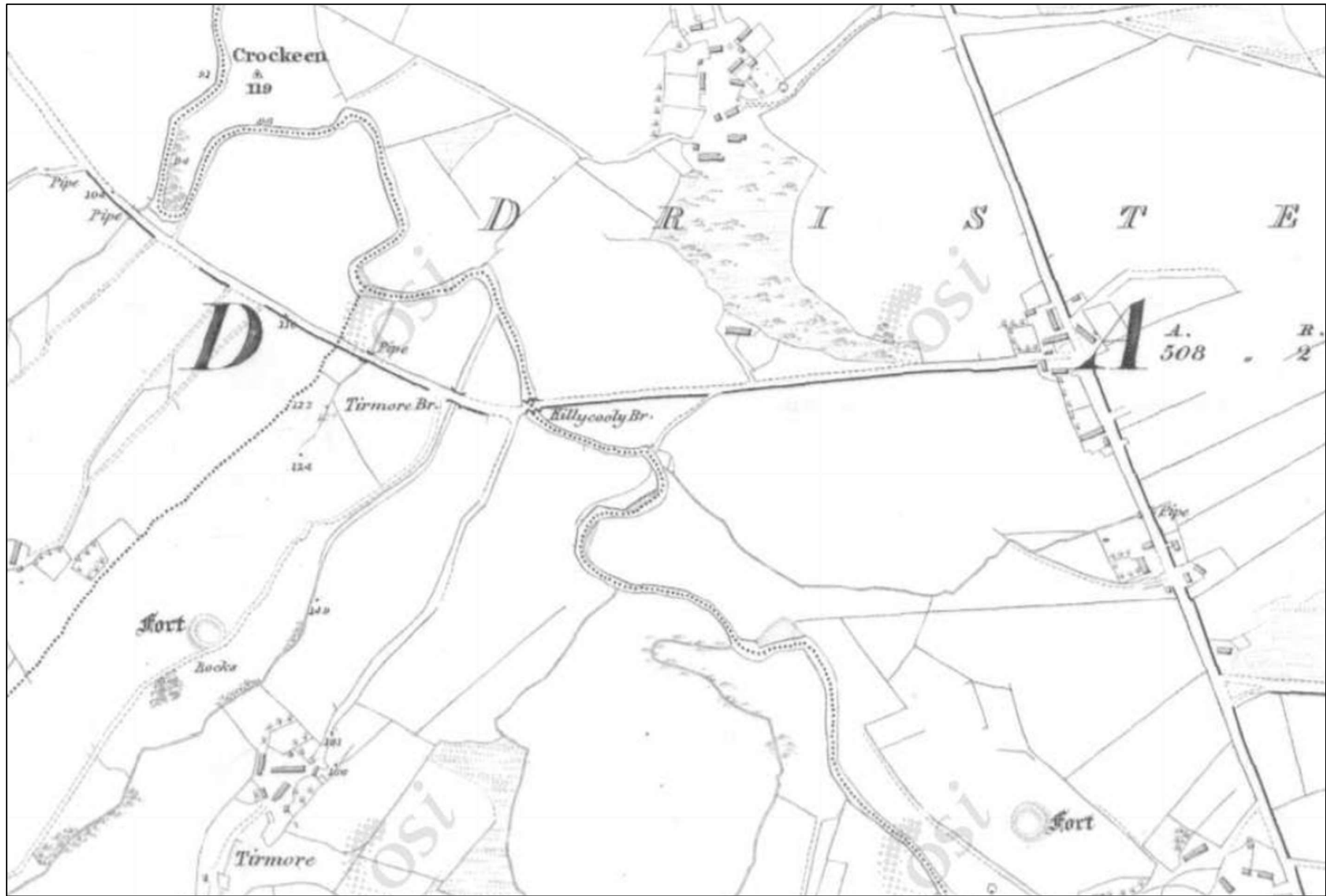
# Appendix D

## OSI 6 INCH MAP & OSI 25 INCH MAP





***Irish Townland and Historical Map - MapGenie 25 Inch – ITM***



*Irish Townland and Historical Map -MapGenie 6 Inch First Edition Black*

# Appendix E

## DONEGAL DEVELOPMENT PLAN 2018-2024



**Draft County Donegal  
Development Plan  
2018 - 2024**

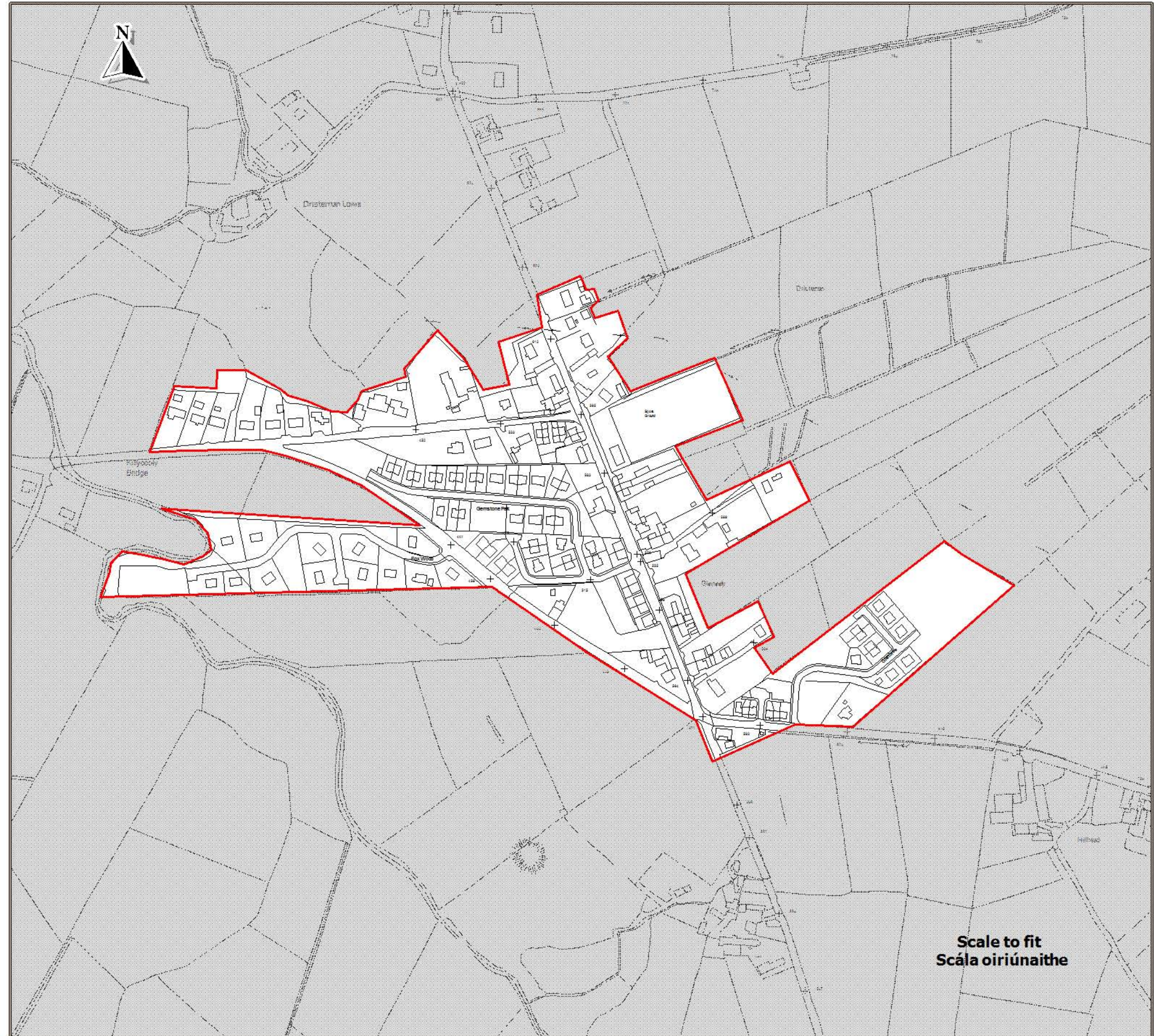
**Dréacht Plean Forbartha  
Contae Dhún na nGall  
2018 - 2024**

Layer 3 - Map 15.41  
Sraith 3 - Léarscáil 15.41

**Gleneely  
Gleann Daoile**

**Settlement Framework  
Creatlach Lonnaíochta**

 Settlement Boundary  
Teorainn Lonnaíochta



Source - Donegal County Council  
Foinse - Comhairle Chontae Dhún na nGall

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Sonraí de chuid Shuirbhéireacht Ordánais Éireann ama atáirgeadh faoi Uimhir Cheadúnais SOÉ 2017/02/CCMA Comhairle Contae Dhún na nGall. Má dhéantar é seo a atáirgeadh gan údarás, sáróidh sé cóipcheart Shuirbhéireacht Ordánais Éireann agus Rialtas na hÉireann. Shuirbhéireacht Ordánais Éireann, 2017. Comhairle Contae Dhún na nGall, 2017.

To be read in conjunction with relevant accompanying text contained in the front section of this appendix as well as other relevant objectives & policies of the CDP.  
Le Léamh i gcomhar leis an téacs ábhartha tionlacain atá chun tosaigh sa chuid seo den aguisin chomh maith le cuspóirí agus beartais ábhartha eile sa PFC.

# Appendix F

## CAUSEWAY FLOW DESIGN REPORT

### Links (Input)

| Name  | US Node | DS Node  | Length (m) | ks (mm) / n | US IL (m) | DS IL (m) | Fall (m) | Slope (1:X) | Dia (mm) | T of C (mins) | Rain (mm/hr) |
|-------|---------|----------|------------|-------------|-----------|-----------|----------|-------------|----------|---------------|--------------|
| 2.000 | SM_01   | SM_02    | 19.244     | 0.600       | 33.900    | 32.800    | 1.100    | 17.5        | 300      | 5.08          | 50.0         |
| 2.001 | SM_02   | SM_03    | 9.973      | 0.600       | 32.800    | 32.240    | 0.560    | 17.8        | 450      | 5.12          | 50.0         |
| 2.002 | SM_03   | SM_04    | 8.760      | 0.600       | 32.240    | 31.775    | 0.465    | 18.8        | 600      | 5.15          | 50.0         |
| 1.000 | SM_06   | SM_05    | 45.520     | 0.600       | 33.200    | 32.800    | 0.400    | 113.8       | 900      | 5.26          | 50.0         |
| 1.001 | SM_05   | SM_04    | 41.578     | 0.600       | 32.800    | 31.775    | 1.025    | 40.6        | 900      | 5.40          | 50.0         |
| 1.003 | SM_07   | Headwall | 16.361     | 0.600       | 31.769    | 31.494    | 0.275    | 59.5        | 300      | 5.68          | 50.0         |
| 1.002 | SM_04   | SM_07    | 4.860      | 0.600       | 31.775    | 31.769    | 0.006    | 810.0       | 300      | 5.55          | 50.0         |

### Manhole Schedule

| Node     | Easting (m) | Northing (m) | CL (m) | Depth (m) | Dia (mm) | Connections | Link  | IL (m) | Dia (mm) |
|----------|-------------|--------------|--------|-----------|----------|-------------|-------|--------|----------|
| SM_01    | 653661.770  | 944114.450   | 35.480 | 1.580     | 1200     |             |       |        |          |
|          |             |              |        |           |          | 0           | 2.000 | 33.900 | 300      |
| SM_02    | 653663.460  | 944095.280   | 34.510 | 1.710     | 1800     |             | 1     | 2.000  | 32.800   |
|          |             |              |        |           |          | 0           | 2.001 | 32.800 | 450      |
| SM_03    | 653669.810  | 944087.590   | 34.040 | 1.800     | 1800     |             | 1     | 2.001  | 32.240   |
|          |             |              |        |           |          | 0           | 2.002 | 32.240 | 600      |
| SM_04    | 653678.570  | 944087.580   | 33.970 | 2.195     | 2400     |             | 1     | 2.002  | 31.775   |
|          |             |              |        |           |          | 2           | 1.001 | 31.775 | 900      |
|          |             |              |        |           |          | 0           | 1.002 | 31.775 | 300      |
| SM_05    | 653720.050  | 944090.440   | 35.000 | 2.200     | 1800     |             | 1     | 1.000  | 32.800   |
|          |             |              |        |           |          | 0           | 1.001 | 32.800 | 900      |
| SM_06    | 653765.460  | 944093.600   | 36.120 | 2.920     | 1800     |             |       |        |          |
|          |             |              |        |           |          | 0           | 1.000 | 33.200 | 900      |
| Headwall | 653664.900  | 944073.730   | 32.000 | 0.506     | 1200     |             | 1     | 1.003  | 31.494   |
|          |             |              |        |           |          |             |       |        |          |
| SM_07    | 653678.570  | 944082.720   | 34.100 | 2.331     | 1200     |             | 1     | 1.002  | 31.769   |
|          |             |              |        |           |          | 0           | 1.003 | 31.769 | 300      |

### Node SM\_04 Online StormBrake™ Control

|                          |        |                         |                          |
|--------------------------|--------|-------------------------|--------------------------|
| Flap Valve               | x      | Design Flow (l/s)       | 8.8                      |
| Replaces Downstream Link | x      | Product Code            | FPM-SB1-01850-00880-1100 |
| Invert Level (m)         | 31.775 | Min Outlet Diameter (m) | 0.150                    |
| Design Depth (m)         | 1.850  | Min Node Diameter (mm)  | 1200                     |

**Results for 2 year +10% CC +10% A Critical Storm Duration. Lowest mass balance: 100.00%**

| Node Event       | US Node  | Peak (mins) | Level (m) | Depth (m) | Inflow (l/s) | Node Vol (m <sup>3</sup> ) | Flood (m <sup>3</sup> ) | Status     |
|------------------|----------|-------------|-----------|-----------|--------------|----------------------------|-------------------------|------------|
| 15 minute winter | SM_01    | 11          | 33.915    | 0.015     | 1.2          | 0.0180                     | 0.0000                  | OK         |
| 15 minute winter | SM_02    | 10          | 32.825    | 0.025     | 4.6          | 0.0696                     | 0.0000                  | OK         |
| 60 minute winter | SM_03    | 46          | 32.531    | 0.291     | 5.7          | 0.7730                     | 0.0000                  | OK         |
| 60 minute winter | SM_04    | 46          | 32.532    | 0.757     | 26.1         | 4.3607                     | 0.0000                  | SURCHARGED |
| 15 minute winter | SM_05    | 11          | 32.849    | 0.049     | 19.2         | 0.1726                     | 0.0000                  | OK         |
| 15 minute winter | SM_06    | 11          | 33.223    | 0.023     | 2.1          | 0.0600                     | 0.0000                  | OK         |
| 30 minute summer | Headwall | 39          | 31.544    | 0.050     | 8.8          | 0.0000                     | 0.0000                  | OK         |
| 30 minute summer | SM_07    | 39          | 31.821    | 0.052     | 8.8          | 0.0583                     | 0.0000                  | OK         |

| Link Event (Upstream Depth) | US Node | Link  | DS Node  | Outflow (l/s) | Velocity (m/s) | Flow/Cap | Link Vol (m <sup>3</sup> ) | Discharge Vol (m <sup>3</sup> ) |
|-----------------------------|---------|-------|----------|---------------|----------------|----------|----------------------------|---------------------------------|
| 15 minute winter            | SM_01   | 2.000 | SM_02    | 1.2           | 0.623          | 0.004    | 0.0387                     |                                 |
| 15 minute winter            | SM_02   | 2.001 | SM_03    | 4.6           | 1.255          | 0.006    | 0.3106                     |                                 |
| 60 minute winter            | SM_03   | 2.002 | SM_04    | 3.8           | 0.099          | 0.002    | 1.8275                     |                                 |
| 60 minute winter            | SM_04   | 1.002 | SM_07    | 8.8           | 0.795          | 0.228    | 0.0543                     |                                 |
| 15 minute winter            | SM_05   | 1.001 | SM_04    | 18.6          | 0.374          | 0.006    | 10.2345                    |                                 |
| 15 minute winter            | SM_06   | 1.000 | SM_05    | 2.0           | 0.247          | 0.001    | 0.3938                     |                                 |
| 30 minute summer            | SM_07   | 1.003 | Headwall | 8.8           | 1.118          | 0.061    | 0.1285                     | 26.3                            |

**Results for 30 year +10% CC +10% A Critical Storm Duration. Lowest mass balance: 100.00%**

| Node Event        | US Node  | Peak (mins) | Level (m) | Depth (m) | Inflow (l/s) | Node Vol (m <sup>3</sup> ) | Flood (m <sup>3</sup> ) | Status     |
|-------------------|----------|-------------|-----------|-----------|--------------|----------------------------|-------------------------|------------|
| 15 minute winter  | SM_01    | 10          | 33.920    | 0.020     | 2.3          | 0.0243                     | 0.0000                  | OK         |
| 60 minute winter  | SM_02    | 58          | 33.185    | 0.385     | 13.3         | 1.0725                     | 0.0000                  | OK         |
| 60 minute winter  | SM_03    | 58          | 33.180    | 0.940     | 14.6         | 2.4963                     | 0.0000                  | SURCHARGED |
| 60 minute winter  | SM_04    | 57          | 33.180    | 1.405     | 41.4         | 8.0882                     | 0.0000                  | SURCHARGED |
| 60 minute winter  | SM_05    | 55          | 33.176    | 0.376     | 31.2         | 1.3255                     | 0.0000                  | OK         |
| 15 minute winter  | SM_06    | 11          | 33.230    | 0.030     | 3.9          | 0.0790                     | 0.0000                  | OK         |
| 30 minute winter  | Headwall | 101         | 31.544    | 0.050     | 8.8          | 0.0000                     | 0.0000                  | OK         |
| 480 minute winter | SM_07    | 328         | 31.821    | 0.052     | 8.8          | 0.0583                     | 0.0000                  | OK         |

| Link Event (Upstream Depth) | US Node | Link  | DS Node  | Outflow (l/s) | Velocity (m/s) | Flow/Cap | Link Vol (m <sup>3</sup> ) | Discharge Vol (m <sup>3</sup> ) |
|-----------------------------|---------|-------|----------|---------------|----------------|----------|----------------------------|---------------------------------|
| 15 minute winter            | SM_01   | 2.000 | SM_02    | 2.3           | 0.755          | 0.008    | 0.4053                     |                                 |
| 60 minute winter            | SM_02   | 2.001 | SM_03    | 9.1           | 1.105          | 0.012    | 1.5094                     |                                 |
| 60 minute winter            | SM_03   | 2.002 | SM_04    | -13.0         | 0.132          | -0.008   | 2.4675                     |                                 |
| 60 minute winter            | SM_04   | 1.002 | SM_07    | 8.8           | 0.795          | 0.228    | 0.0543                     |                                 |
| 60 minute winter            | SM_05   | 1.001 | SM_04    | 19.5          | 0.332          | 0.006    | 18.3902                    |                                 |
| 15 minute winter            | SM_06   | 1.000 | SM_05    | 3.8           | 0.296          | 0.002    | 1.8816                     |                                 |
| 480 minute winter           | SM_07   | 1.003 | Headwall | 8.8           | 1.118          | 0.061    | 0.1285                     | 133.9                           |



**Results for 100 year +10% CC +10% A Critical Storm Duration. Lowest mass balance: 100.00%**

| Node Event        | US Node  | Peak (mins) | Level (m) | Depth (m) | Inflow (l/s) | Node Vol (m <sup>3</sup> ) | Flood (m <sup>3</sup> ) | Status     |
|-------------------|----------|-------------|-----------|-----------|--------------|----------------------------|-------------------------|------------|
| 15 minute winter  | SM_01    | 10          | 33.922    | 0.022     | 3.0          | 0.0274                     | 0.0000                  | OK         |
| 120 minute winter | SM_02    | 94          | 33.438    | 0.638     | 7.1          | 1.7800                     | 0.0000                  | SURCHARGED |
| 120 minute winter | SM_03    | 96          | 33.436    | 1.196     | 7.1          | 3.1754                     | 0.0000                  | SURCHARGED |
| 120 minute winter | SM_04    | 96          | 33.435    | 1.660     | 31.6         | 9.5564                     | 0.0000                  | SURCHARGED |
| 120 minute winter | SM_05    | 96          | 33.429    | 0.629     | 30.9         | 2.2188                     | 0.0000                  | OK         |
| 120 minute winter | SM_06    | 98          | 33.434    | 0.234     | 7.7          | 0.6171                     | 0.0000                  | OK         |
| 60 minute summer  | Headwall | 160         | 31.544    | 0.050     | 8.8          | 0.0000                     | 0.0000                  | OK         |
| 15 minute winter  | SM_07    | 93          | 31.821    | 0.052     | 8.8          | 0.0583                     | 0.0000                  | OK         |

| Link Event (Upstream Depth) | US Node | Link  | DS Node  | Outflow (l/s) | Velocity (m/s) | Flow/Cap | Link Vol (m <sup>3</sup> ) | Discharge Vol (m <sup>3</sup> ) |
|-----------------------------|---------|-------|----------|---------------|----------------|----------|----------------------------|---------------------------------|
| 15 minute winter            | SM_01   | 2.000 | SM_02    | 3.0           | 0.825          | 0.011    | 0.6905                     |                                 |
| 120 minute winter           | SM_02   | 2.001 | SM_03    | 5.7           | 1.017          | 0.007    | 1.5802                     |                                 |
| 120 minute winter           | SM_03   | 2.002 | SM_04    | 7.7           | 0.101          | 0.005    | 2.4675                     |                                 |
| 120 minute winter           | SM_04   | 1.002 | SM_07    | 8.8           | 0.795          | 0.228    | 0.0543                     |                                 |
| 120 minute winter           | SM_05   | 1.001 | SM_04    | -16.5         | 0.278          | -0.005   | 23.0224                    |                                 |
| 120 minute winter           | SM_06   | 1.000 | SM_05    | -6.2          | 0.230          | -0.003   | 13.7484                    |                                 |
| 15 minute winter            | SM_07   | 1.003 | Headwall | 8.8           | 1.118          | 0.061    | 0.1285                     | 52.1                            |

# Appendix G

## DRAINAGE DRAWINGS



| REV | DESCRIPTION | BY | CHK | APP | DATE |
|-----|-------------|----|-----|-----|------|
|     |             |    |     |     |      |

Donegal County Council

**FOYLE CONSULTING ENGINEERS**  
 HARBOUR OFFICE, PORT ROAD  
 LISAHALLY  
 L'DERRY, BT47 6FL

TEL: +44 (0)28 71865757  
 FAX: +44 (0)28 71861656  
 e-mail: admin@foylece.com

Project:  
 Carn Road, Gleneely, Co. Donegal

Drawing Title:  
 Q100 Flood Plain Plan

| Scale @     | Drawn       | Date     | Checked | Date   |
|-------------|-------------|----------|---------|--------|
| A1          | BMcl        | Oct 23   | BMcl    | Oct 23 |
| Project No. | Drawing No. | Revision |         |        |
| F2941       | 003         |          |         |        |

# Appendix H

## PROPOSED SITE LAYOUT



| REV | DESCRIPTION | BY | CHK | APP | DATE |
|-----|-------------|----|-----|-----|------|
|     |             |    |     |     |      |

Donegal County Council

**FOYLE CONSULTING ENGINEERS**  
 HARBOUR OFFICE, PORT ROAD  
 LISAHALLY  
 L'DERRY, BT47 6FL

TEL: +44 (0)28 71865757  
 FAX: +44 (0)28 71861656  
 e-mail: admin@foylece.com

Project:  
Carn Road, Gleneely, Co. Donegal

Drawing Title:  
Proposed Site Layout

|                      |                    |                |                 |                |
|----------------------|--------------------|----------------|-----------------|----------------|
| Scale @ A1<br>1:500  | Drawn<br>BMcl      | Date<br>Oct 23 | Checked<br>BMcl | Date<br>Oct 23 |
| Project No.<br>F2941 | Drawing No.<br>002 | Revision       |                 |                |

# Appendix I

## TOPOGRAPHICAL SURVEY



| REV | DESCRIPTION | BY | CHK | APP | DATE |
|-----|-------------|----|-----|-----|------|
|     |             |    |     |     |      |

Donegal County Council

**FOYLE CONSULTING ENGINEERS**  
 HARBOUR OFFICE, PORT ROAD  
 LISAHALLY  
 L'DERRY, BT47 6FL  
 TEL: +44 (0)28 71865757  
 FAX: +44 (0)28 71861656  
 e-mail: admin@foylece.com

Project:  
Carn Road, Gleneely, Co. Donegal

Drawing Title:  
Site Layout

| Scale @     | Drawn       | Date     | Checked | Date   |
|-------------|-------------|----------|---------|--------|
| A1          | BMcl        | Oct 23   | BMcl    | Oct 23 |
| Project No. | Drawing No. | Revision |         |        |
| F2941       | 001         |          |         |        |